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Radiometric quantities and their measurement

Ken Voss, Ocean Optics Class, Darling Center, Maine
Summer, 2013

While radiance is the fundamental property, for measurements, an irradiance detector is easier to understand, so I will build from irradiance to radiance.

Outline

- 1) Spectral resolution of Detectors
- 2) Plane irradiance measurements
- 3) Scalar irradiance measurements
- 4) Radiance and Radiance
Distribution measurements

Two (maybe three) classes of detectors/
instruments if defined by spectral resolution

1) Multi-channel instruments

2) Hyperspectral instruments

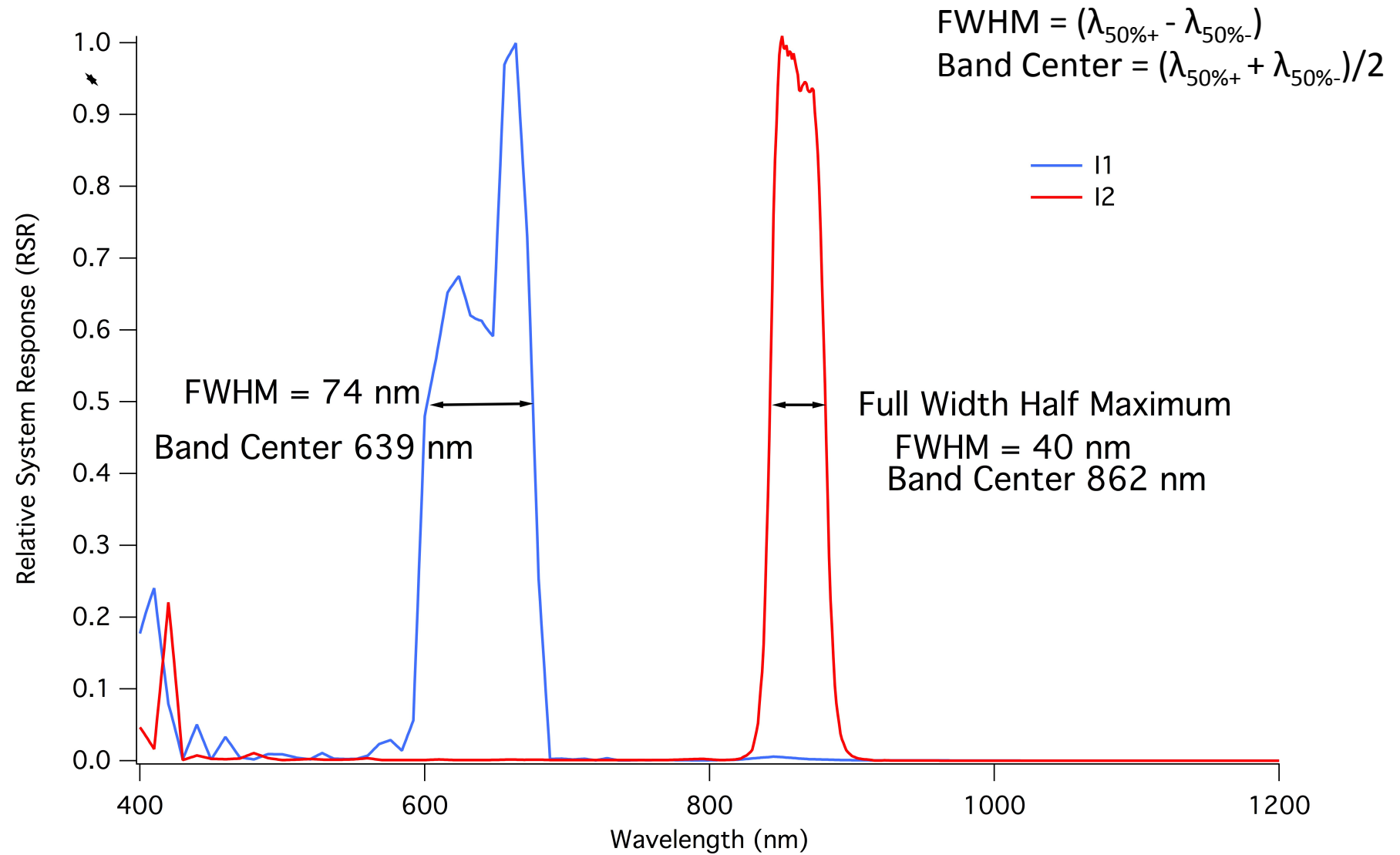
3) PAR (or other broadband for example UV-A) sensor

Narrow band, multi channel instruments

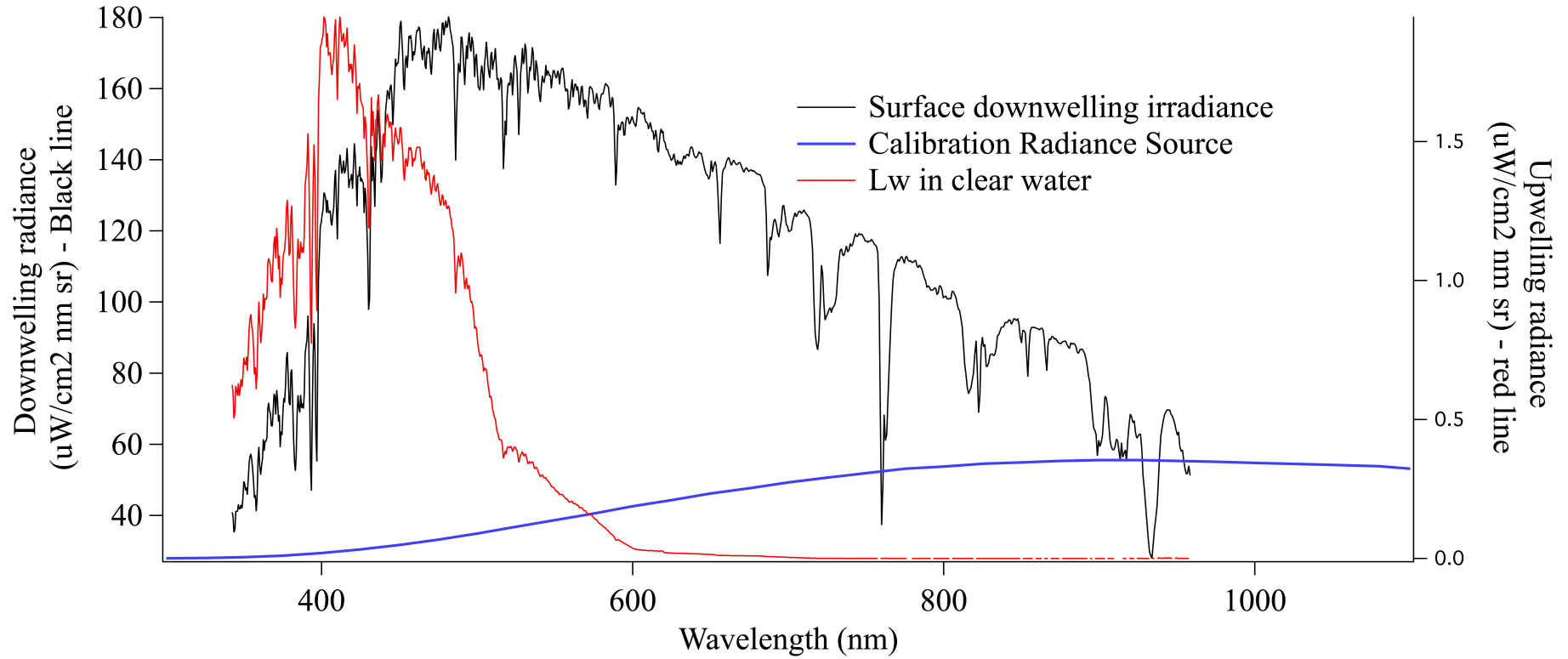
- 1) Typically channels have spectral bands of 10nm wide.
 - a) Most ocean optics parameters do not have sharp features.
 - b) May try to match some other spectral shape (SeaWiFS bands).

- 2) Spectral channels defined by filters, typically interference filters.
 - a) Filters have some spectral shape, defined by band center and the width.
 - b) Have to be careful of out-of-band effects (looking at different “color” sources)

Detectors

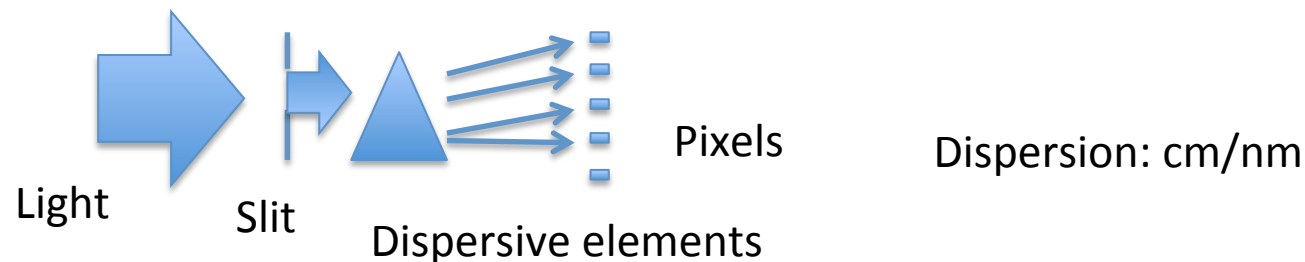


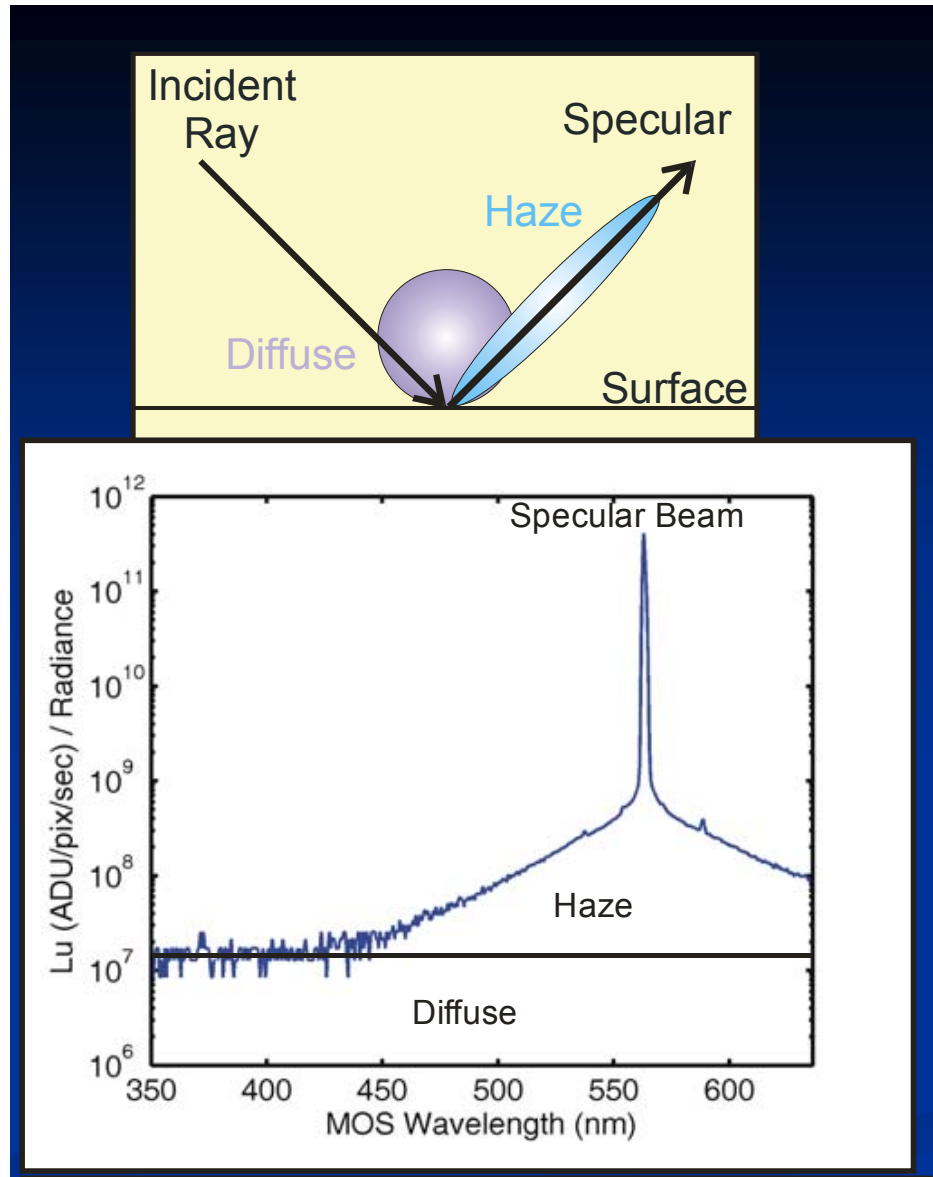
Detectors



Hyperspectral Detectors

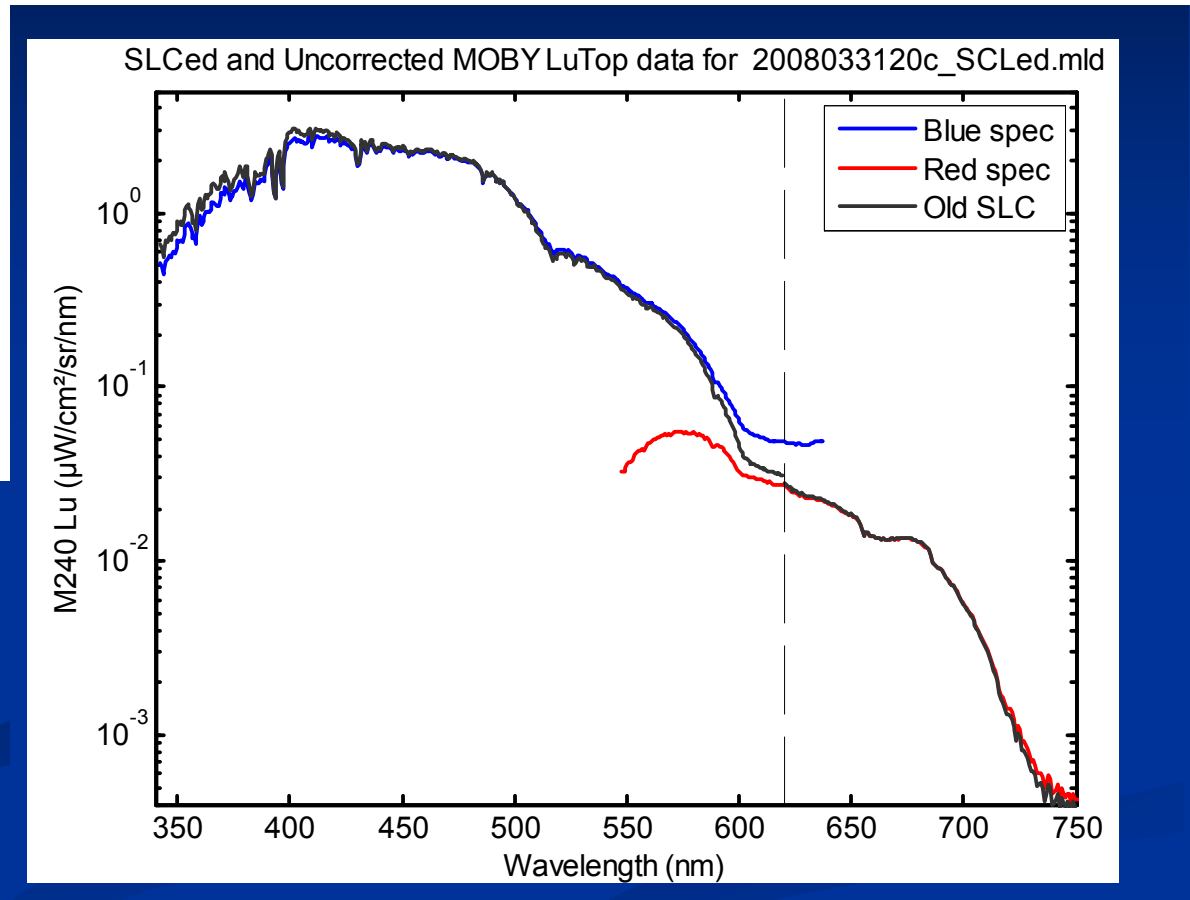
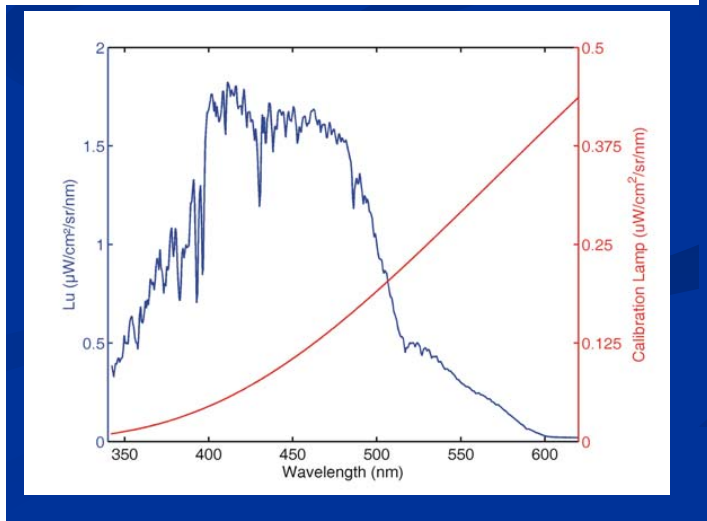
- 1) “continuous spectrum”, really channels every 1-10nm.
- 2) Typically grating or prism dispersive elements.
- 3) Can build integrated channels, match satellite sensor channels, etc.
- 3) Be careful of various effects
 - a) similar to out-of-band effects, have scattered light effects
 - b) resolution limits (entrance slitwidth, dispersion, imaging ability)
just because there is a detector every 1 nm, doesn't mean it tells you anything. Example: WISP reports every 0.3 nm, BW 5 nm.





From Stephanie Flora
Moby project

Detectors



PAR or other broadband (UVA, UVB, etc.)

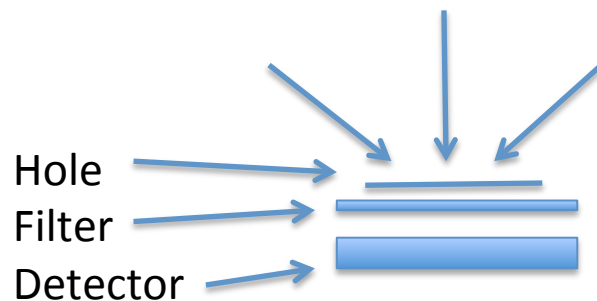
PAR:

- 1) photosynthetically available radiation, try to count photons in the range from 400-700 nm, equal weight to each photon.
- 2) Silicon detector through photoelectric effect, should sort of do this:
Each photon generates one photo-electron (perfect quantum efficiency)
- 3) Problems due to scattering in detector, reabsorption of photo-electrons, spectrally dependent reflection...break down this relationship which then causes calibration to be difficult (different colored sources). Physically not a “nice” measurement, but easy.

Definition of plane Irradiance : $E_d \equiv \frac{\Delta Q}{\Delta t \Delta A \Delta \lambda} \left[\frac{\text{W}}{\text{m}^2 \text{ nm}} \right]$

$$E_d(\theta, \phi, \lambda) \equiv \int_{UH} L(\Omega, \lambda) |\cos \theta| d\Omega = \int_0^{2\pi} \int_0^{\pi/2} L(\theta, \phi, \lambda) |\cos \theta| \sin \theta d\theta d\phi$$

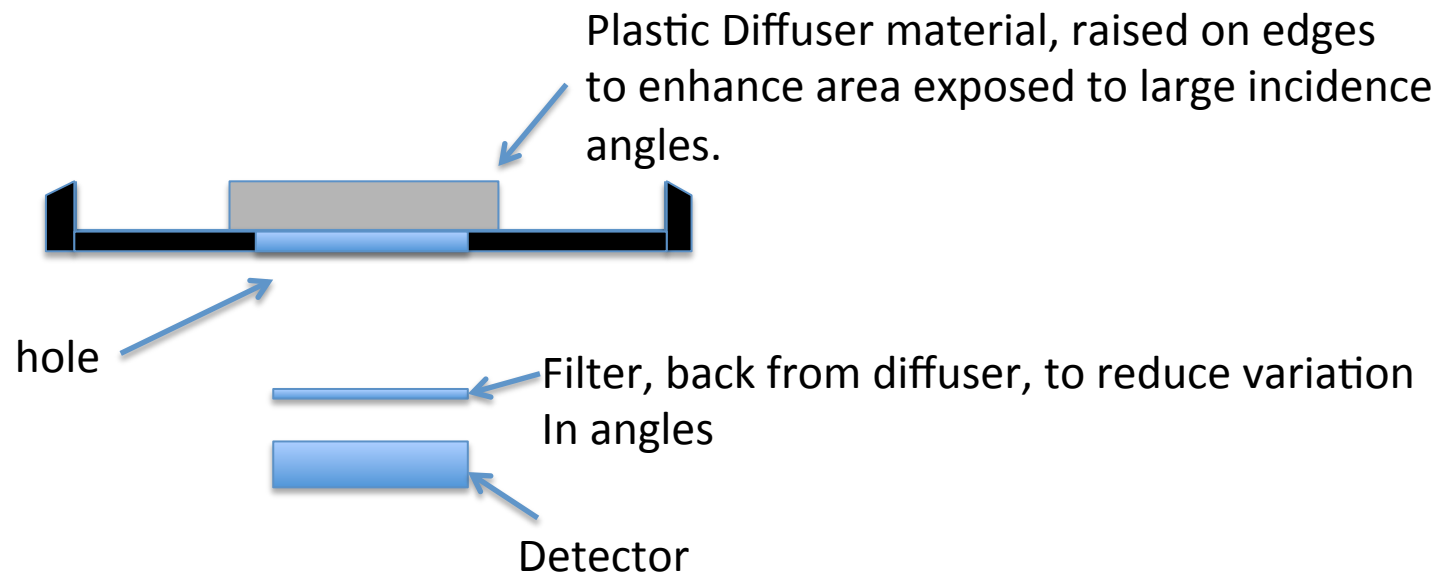
Perfect detector would be a hole, with a detector right behind that collects all the light which passed through the hole:



Problems:

- 1) Filter, typically interference filter, has an angle dependence on spectral transmission
- 2) Detectors also have angular dependence on their response
- 3) Invariably need some sort of window in front of hole, which then has a reflection/transmission coefficient which varies with incident angle. Typically 2-3 decrease with increasing incidence angle.

Real Irradiance detectors try to enhance response to light at large incidence angles. Typical design shown below:



Note: this is in air, not water, but is typical

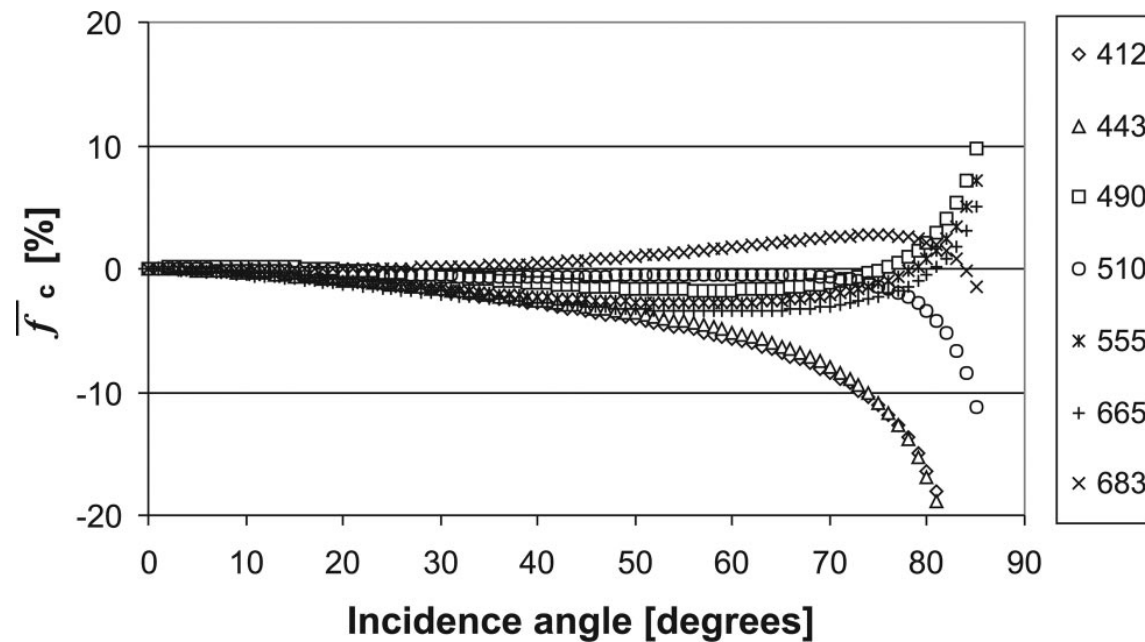
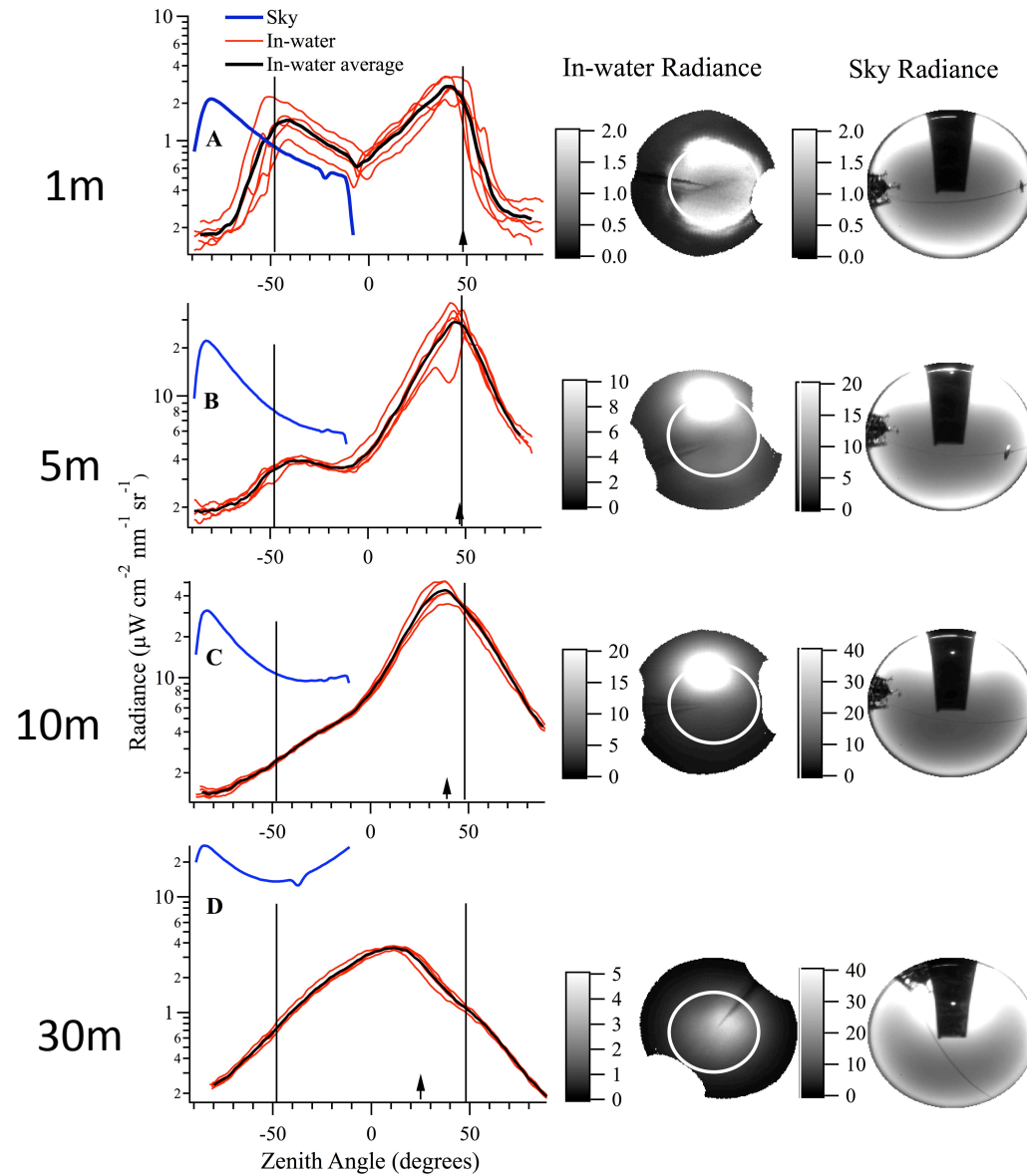


Fig. 3. Average cosine errors $\bar{f}_c(\theta, \lambda)$ determined at various center wavelengths.

Zibordi and Bulgarelli, AO, pg:5529-5538 (2007)

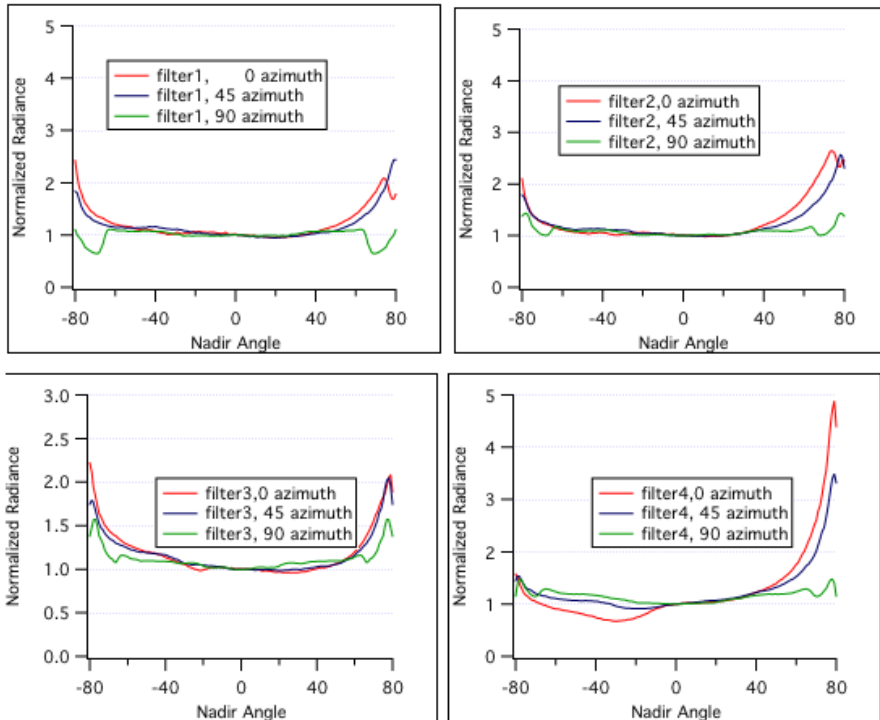
Irradiance

Downwelling Radiance distribution

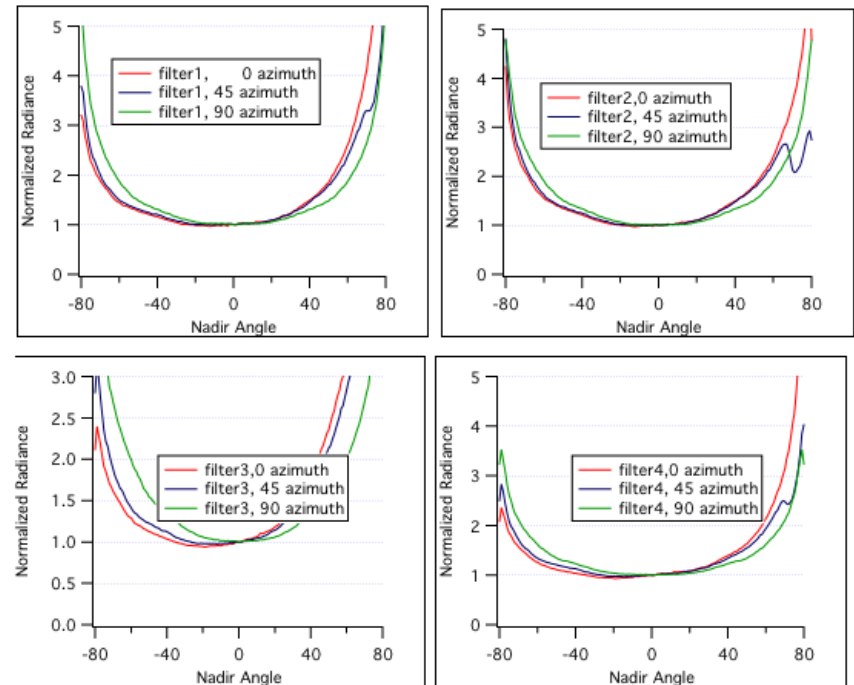


Upwelling Radiance distribution

Low Chl



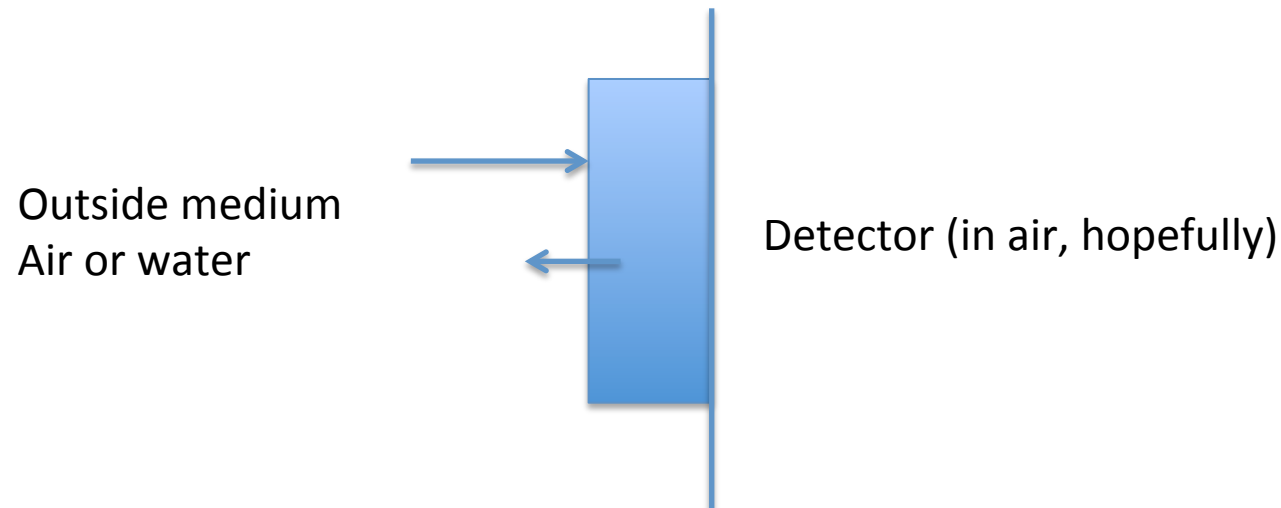
High Chl



Error due to cosine collector much more significant

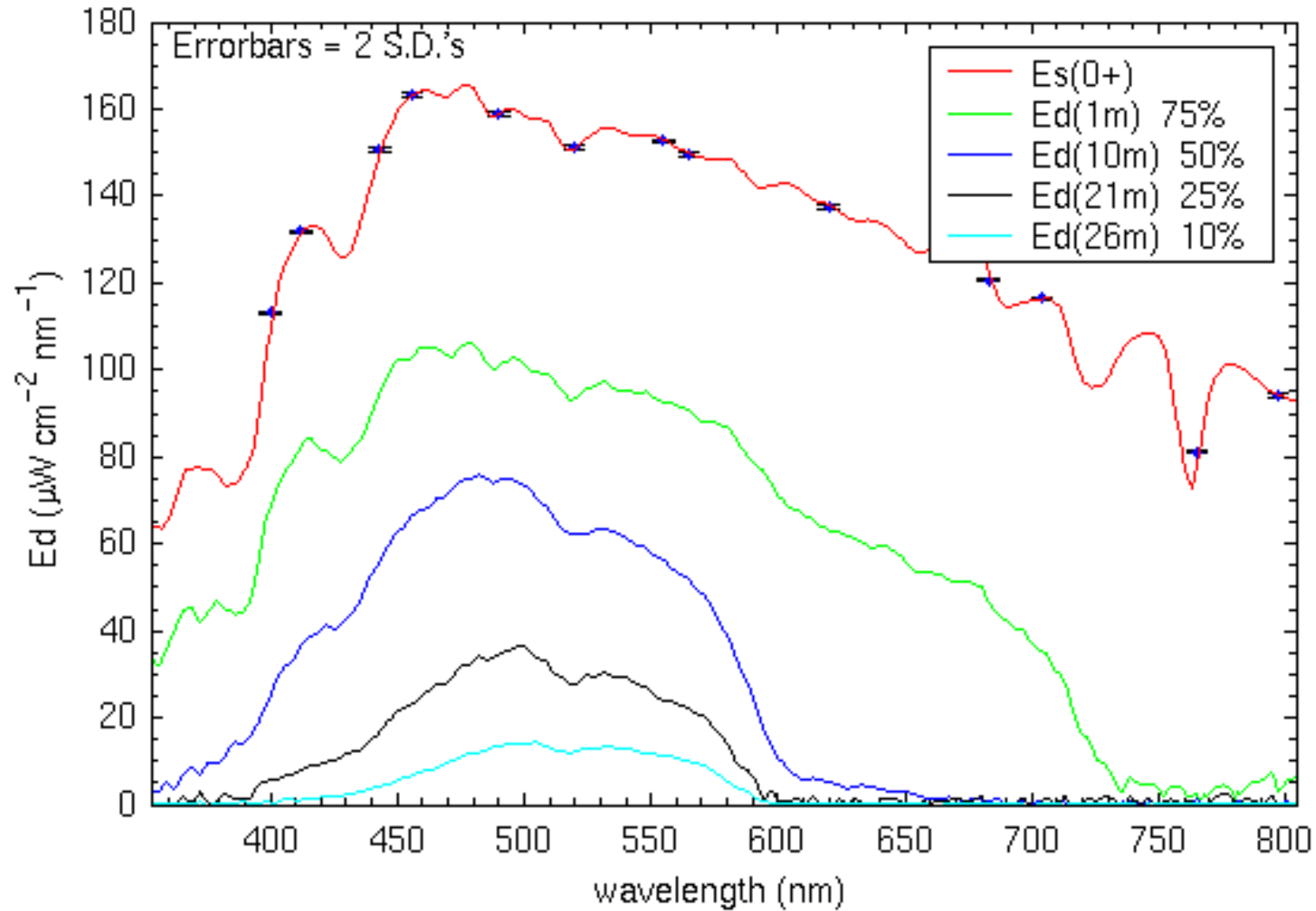
Should mention one more factor: Immersion coefficient, 30-40% correction.

Cosine collector efficiency different when operating in air or water



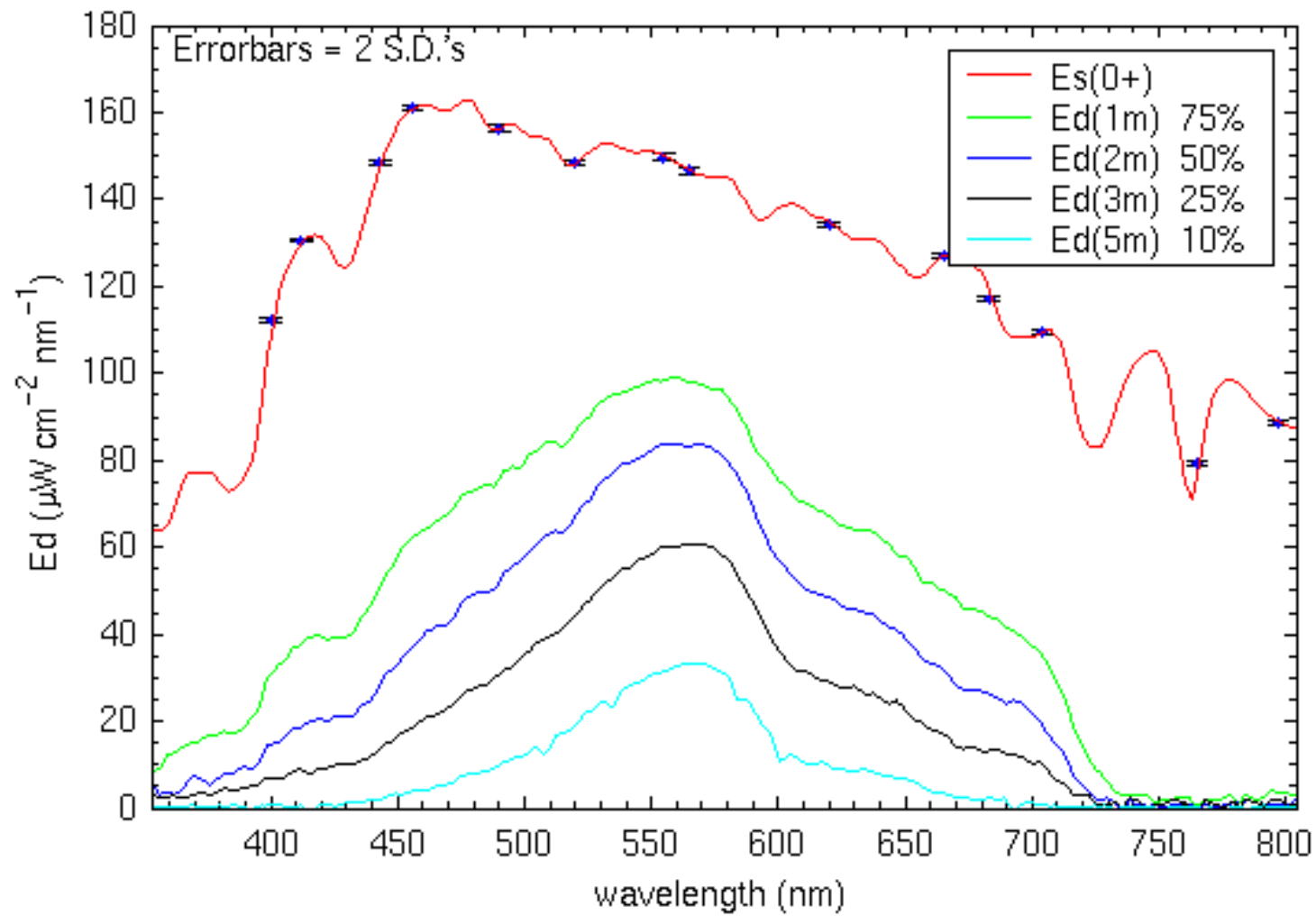
Just drew normal incidence, really all over the place. When in air, larger index of refraction difference between medium and plastic, harder for light to escape. In water more light, after being diffused in detector, can escape....so collection efficiency is less. Immersion factor corrects for this. Is spectrally dependent, and collector design dependent (including plastic), so must be measured. Paper by Hooker and Zibordi 2005.

Irradiance



Blue water station (Data from Marlon Lewis, Satlantic)

Irradiance

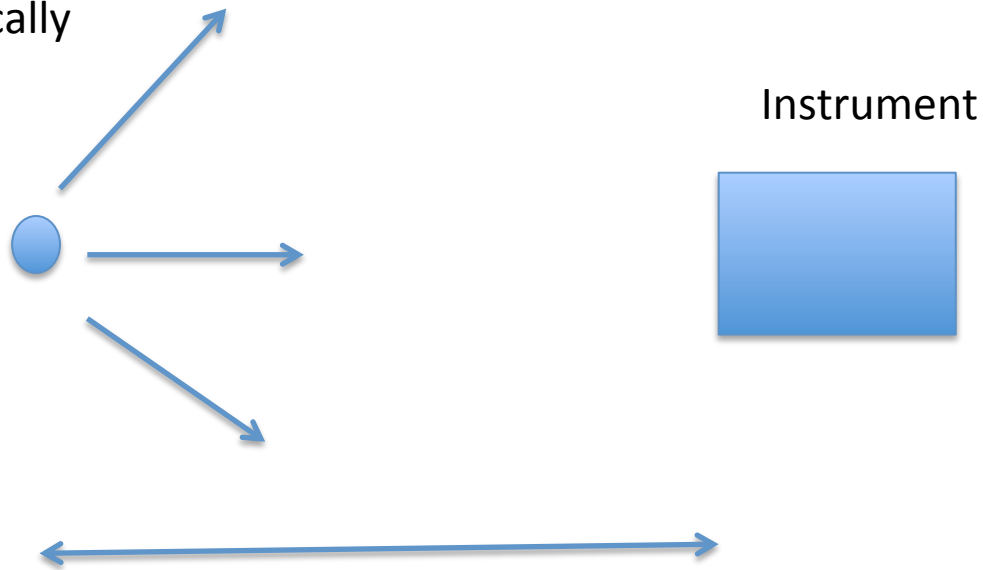


Green water station (Data from Marlon Lewis, Satlantic)

Irradiance

Greatly simplified, but to calibrate this sensor...set up in lab with known source of irradiance:

Known
Source, typically
NIST lamp



Specified distance (typically 50 100 cm), note $1/r^2$ dependence

Definition of Scalar Irradiance: $E_{0d} \equiv \frac{\Delta Q}{\Delta t \Delta A \Delta \lambda} \left[\frac{\text{W}}{\text{m}^2 \text{ nm}} \right]$

$$E_{0d}(\theta, \phi, \lambda) \equiv \int_{UH} L(\Omega, \lambda) d\Omega = \int_0^{2\pi} \int_0^{\pi/2} L(\theta, \phi, \lambda) \sin \theta d\theta d\phi$$

Want to collect all light coming to a single point, regardless of angle. Perfect collector would be as shown earlier, with the limit of the radius going to zero:

(from Curt's Book)

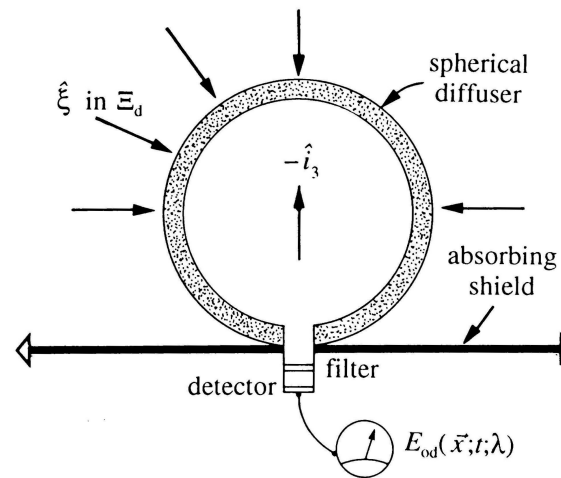


Fig. 1.7. Schematic design of an instrument for measuring spectral scalar irradiance.

Problems:

Would like shield below the ball to be zero (to measure total), or infinity, to measure E_{od} . If you want total then how to handle horizon from a combination of E_{od} and E_{ou} in this case?

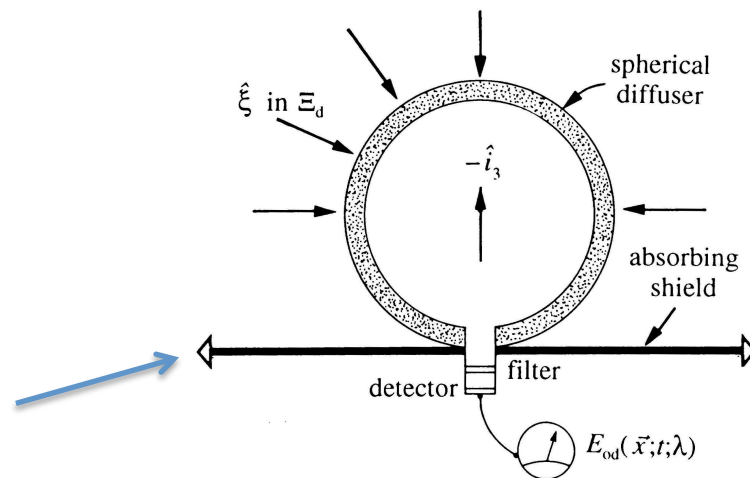


Fig. 1.7. Schematic design of an instrument for measuring spectral scalar irradiance.

Scalar irradiance

$$\mu = E_d / E_o$$

Depth	$E_d(z)$	$E_{od}(z)$	$E_u(z)$	$E_{ou}(z)$	$\mu_d(z)$	$\mu_u(z)$
20.0 m	16.7	23.1	0.488	1.29	0.72	0.38
24.8m	9.34	13.0	0.330	0.852	0.72	0.39
29.9m	6.29	8.78	0.212	0.550	0.72	0.38
44.8m	1.73	2.31	0.0658	0.160	0.75	0.41
49.6	1.56	2.07	0.0512	0.129	0.75	0.40

E_d, E_{od}, E_u, E_{ou} all in units of $\mu\text{W cm}^{-2} \text{nm}^{-1}$

upwelling measurements at 505 nm

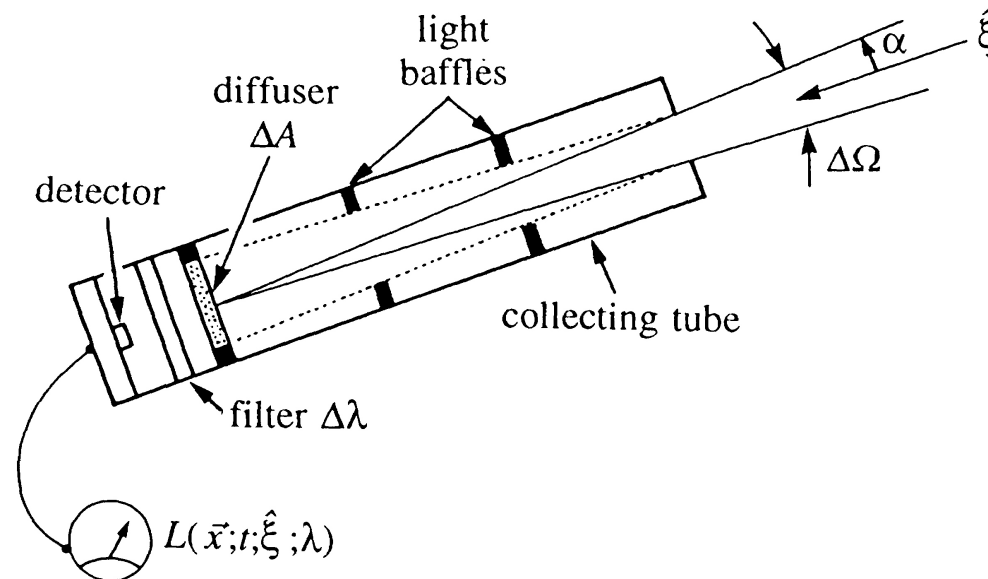
Downwelling measurements at 503 nm

Average cosine of downwelling points to 44 deg, while upwelling is 67 deg

Definition of Radiance:

$$L(\vec{x}, t, \phi, \theta, \lambda) \equiv \frac{\Delta Q}{\Delta t \Delta A \Delta \Omega \Delta \lambda} \left[\frac{\text{J}}{\text{s m}^2 \text{ sr nm}} = \frac{\text{W}}{\text{m}^2 \text{ sr nm}} \right]$$

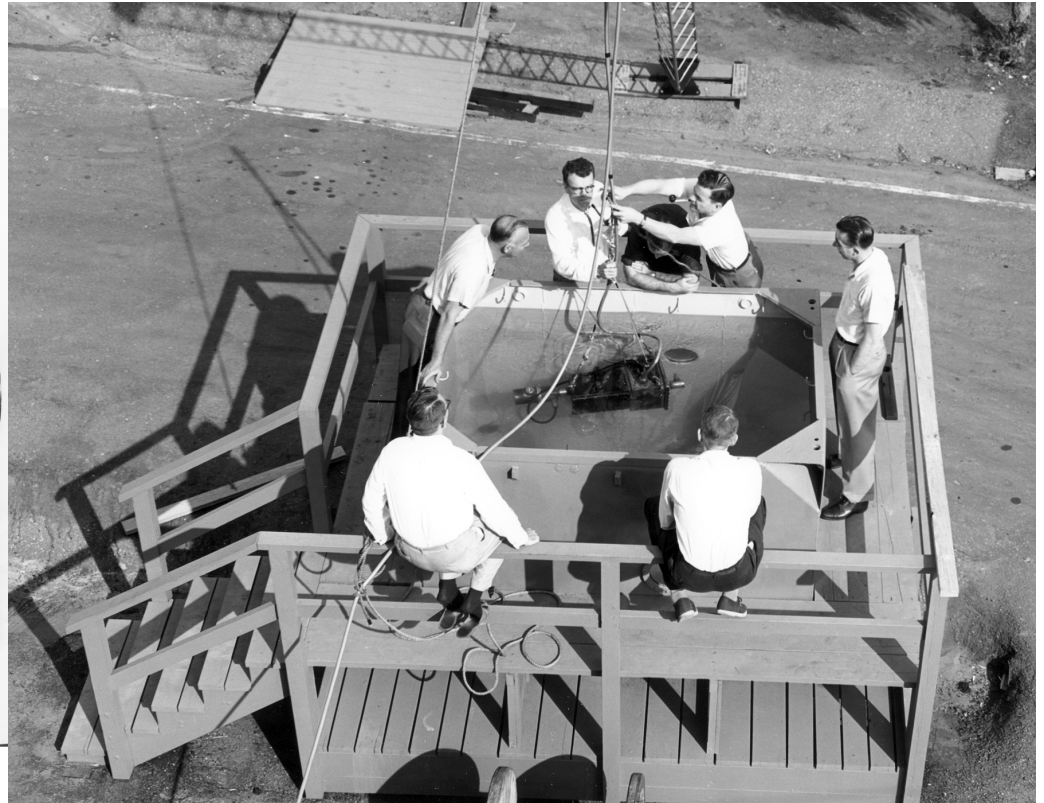
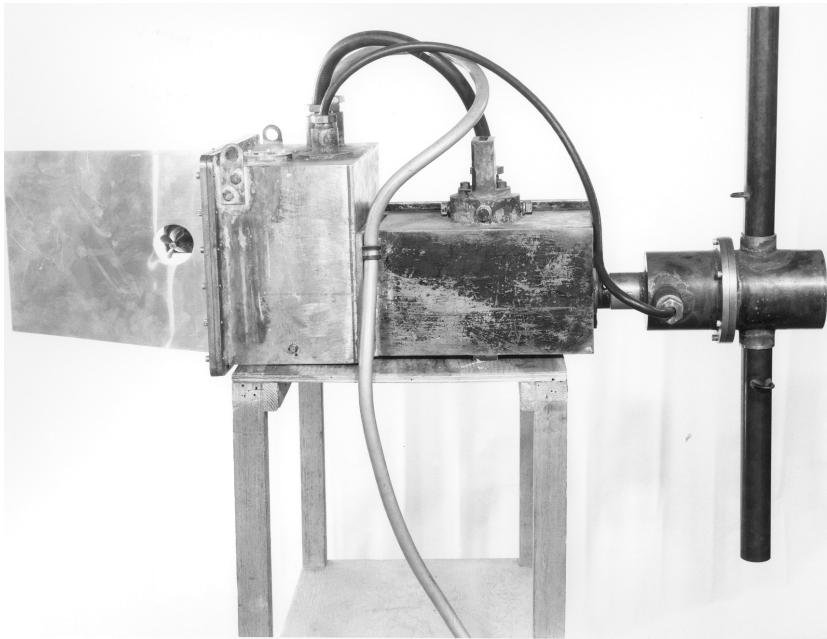
As shown earlier, basic concept for radiometer is a Gershun tube:



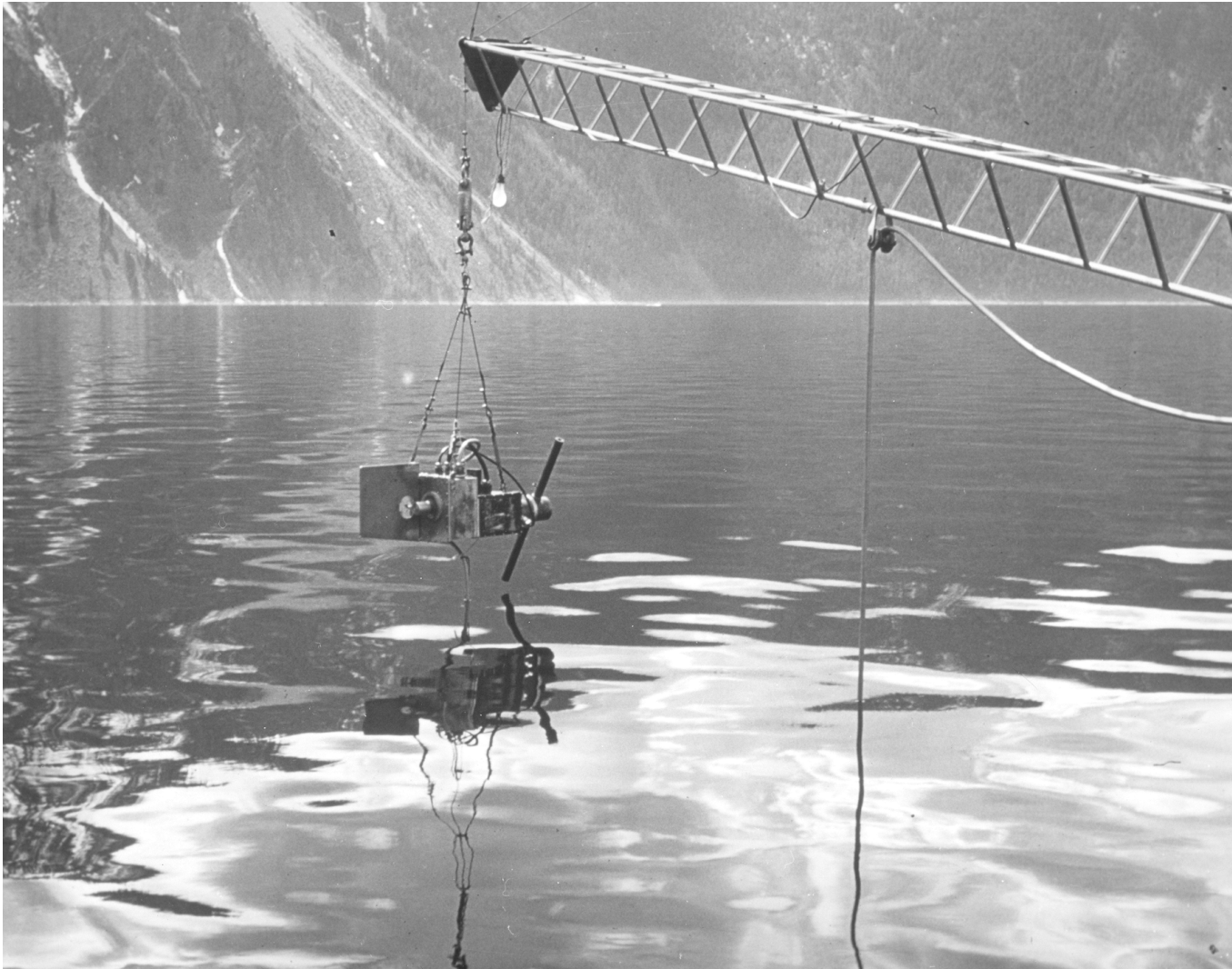
Most often Radiance measured with some sort of Gershun tube device in a single direction (typically upwelling nadir).

But to use radiance in all the other equations, need radiance distribution. Either measure many individual directions (such as Tyler, 1960) or many directions at once with a camera and lens of some sort (Fisheye, Smith et al. 1970).

Example instruments, Tyler :



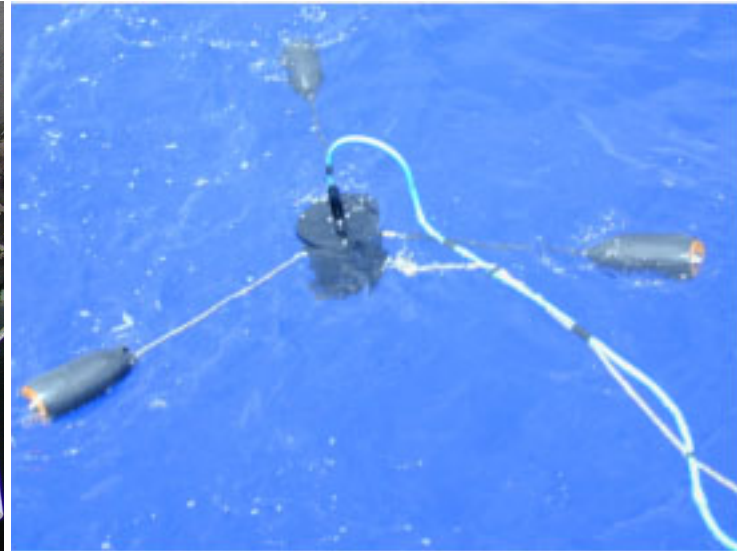
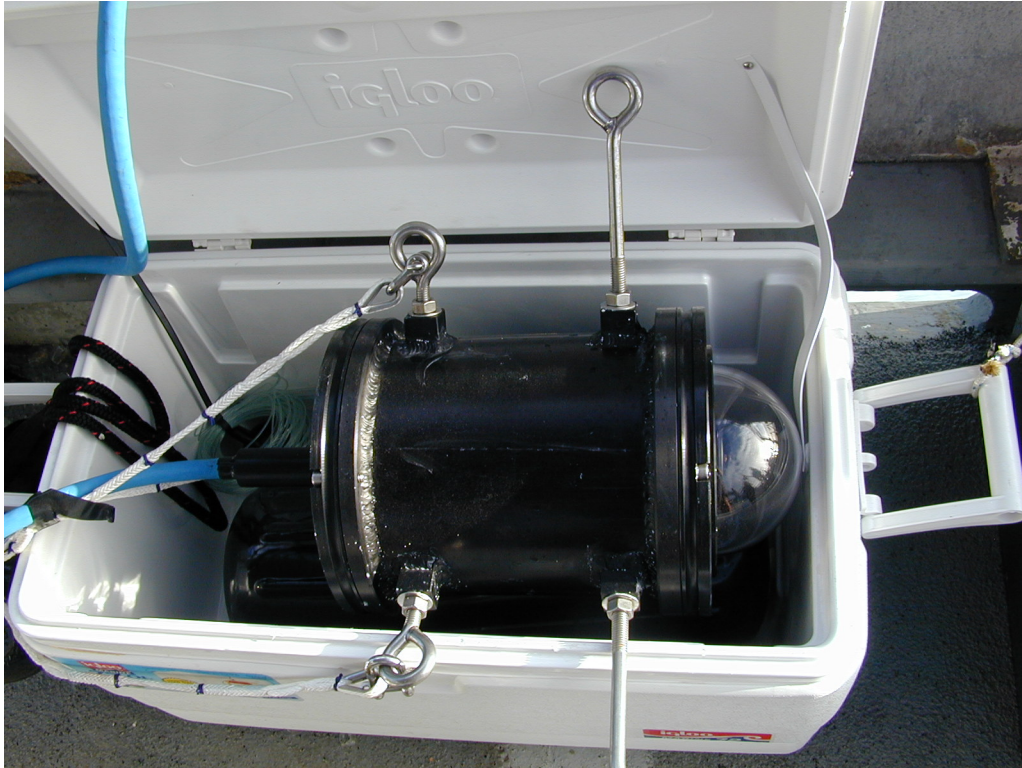
Radiance



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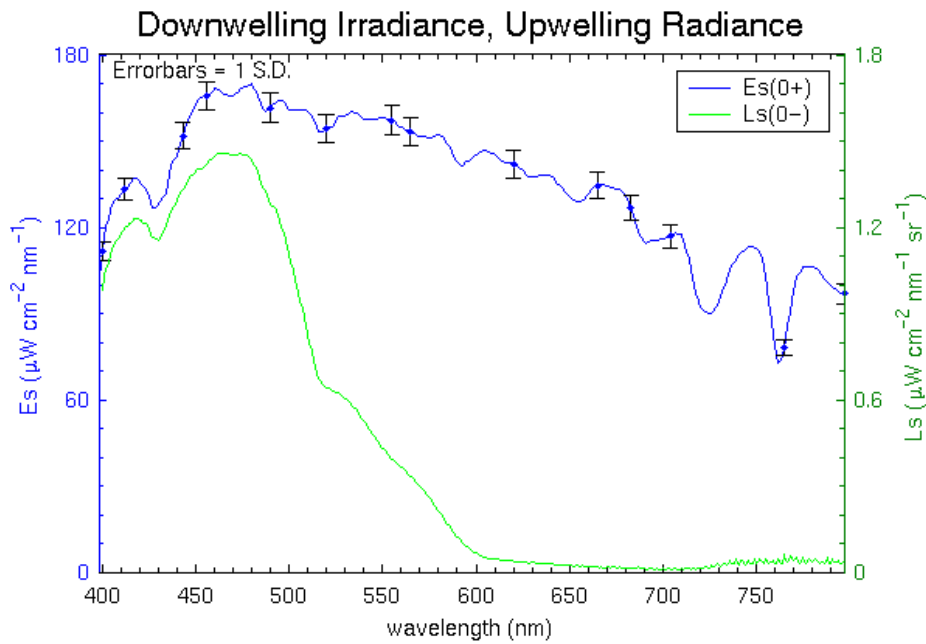


More modern instrument, NuRADS

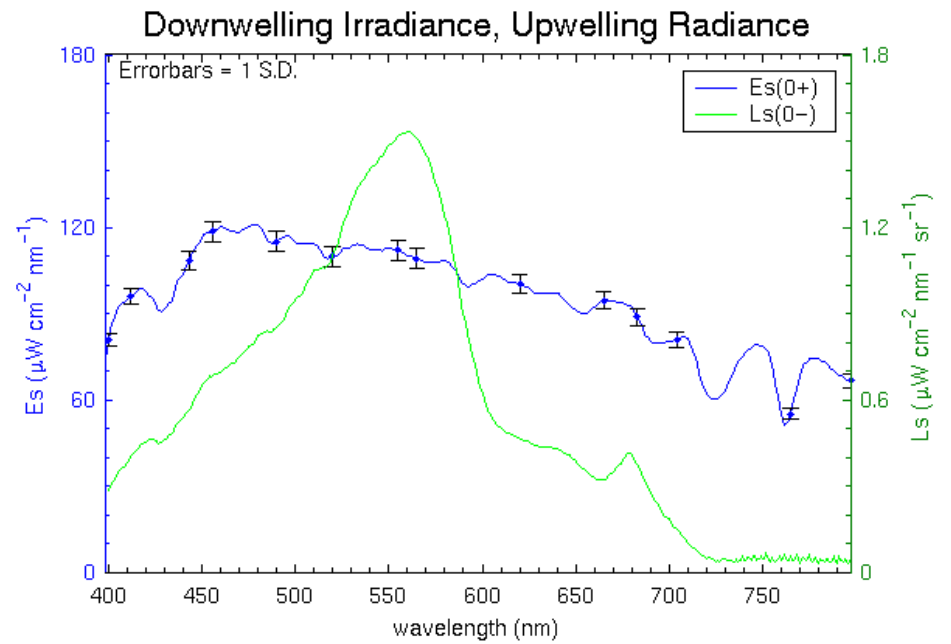


Example Nadir Radiance

Blue water station



Green water station



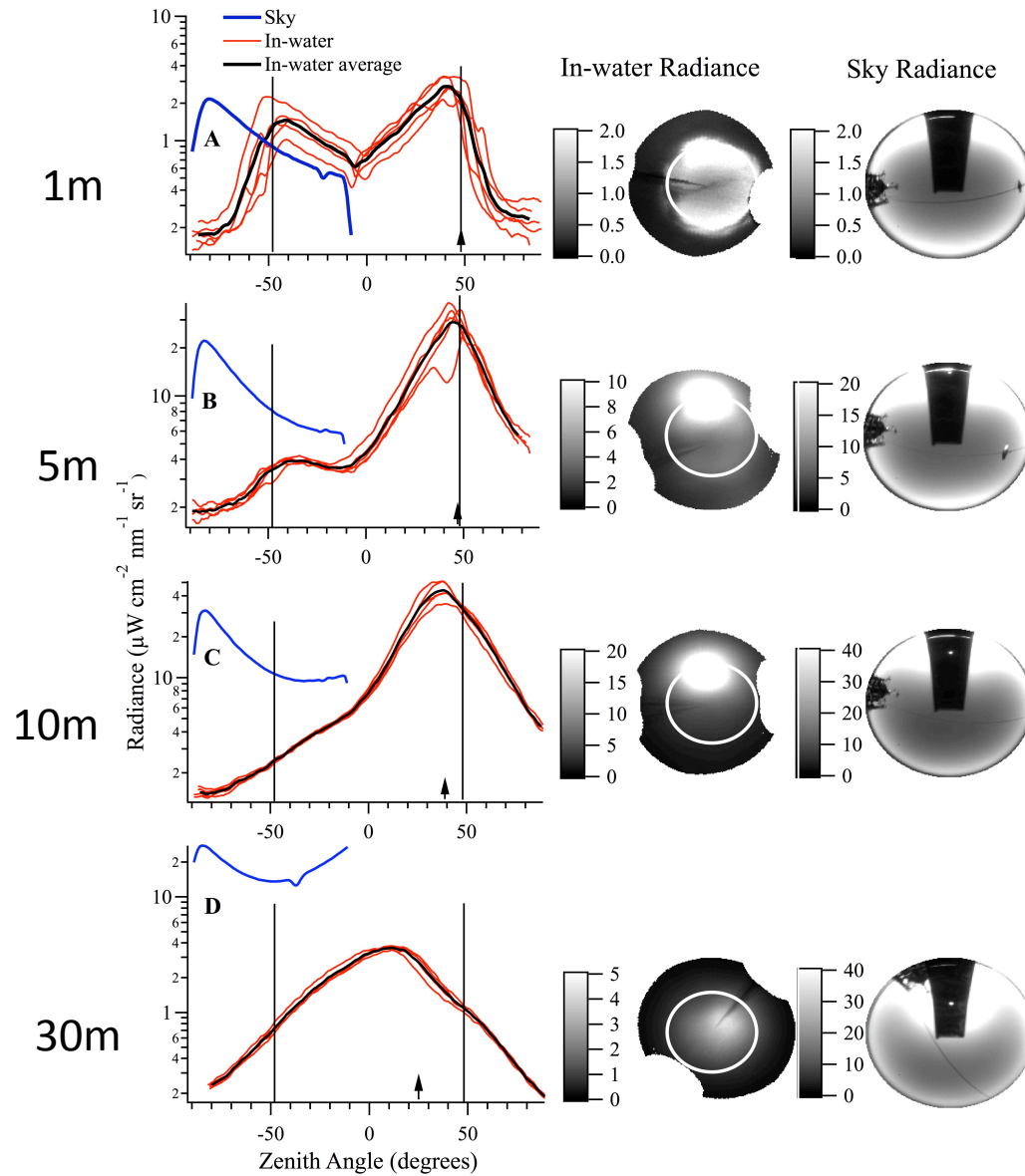
Data from Marlon Lewis



Radiance Distribution

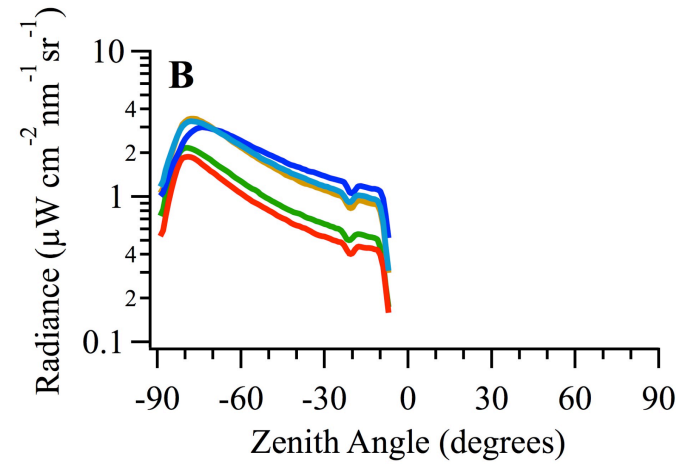
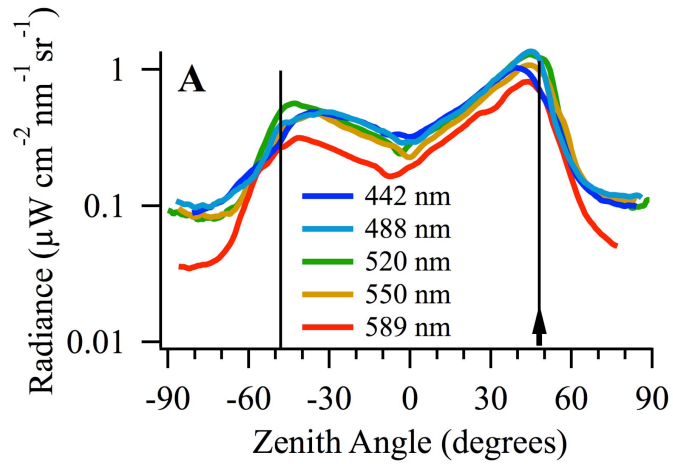
Downwelling
Radiance
Distribution
(520 nm)

Santa Barbara channel

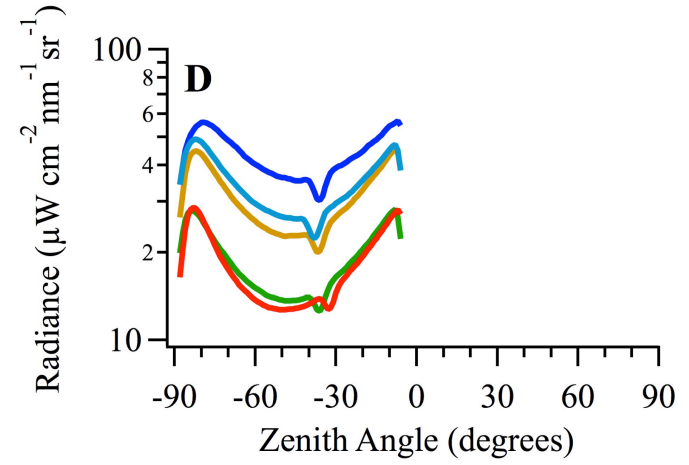
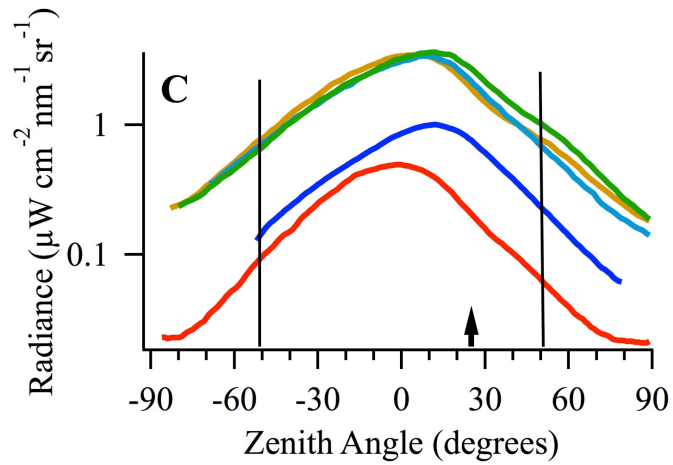


Radiance Distribution

1 m

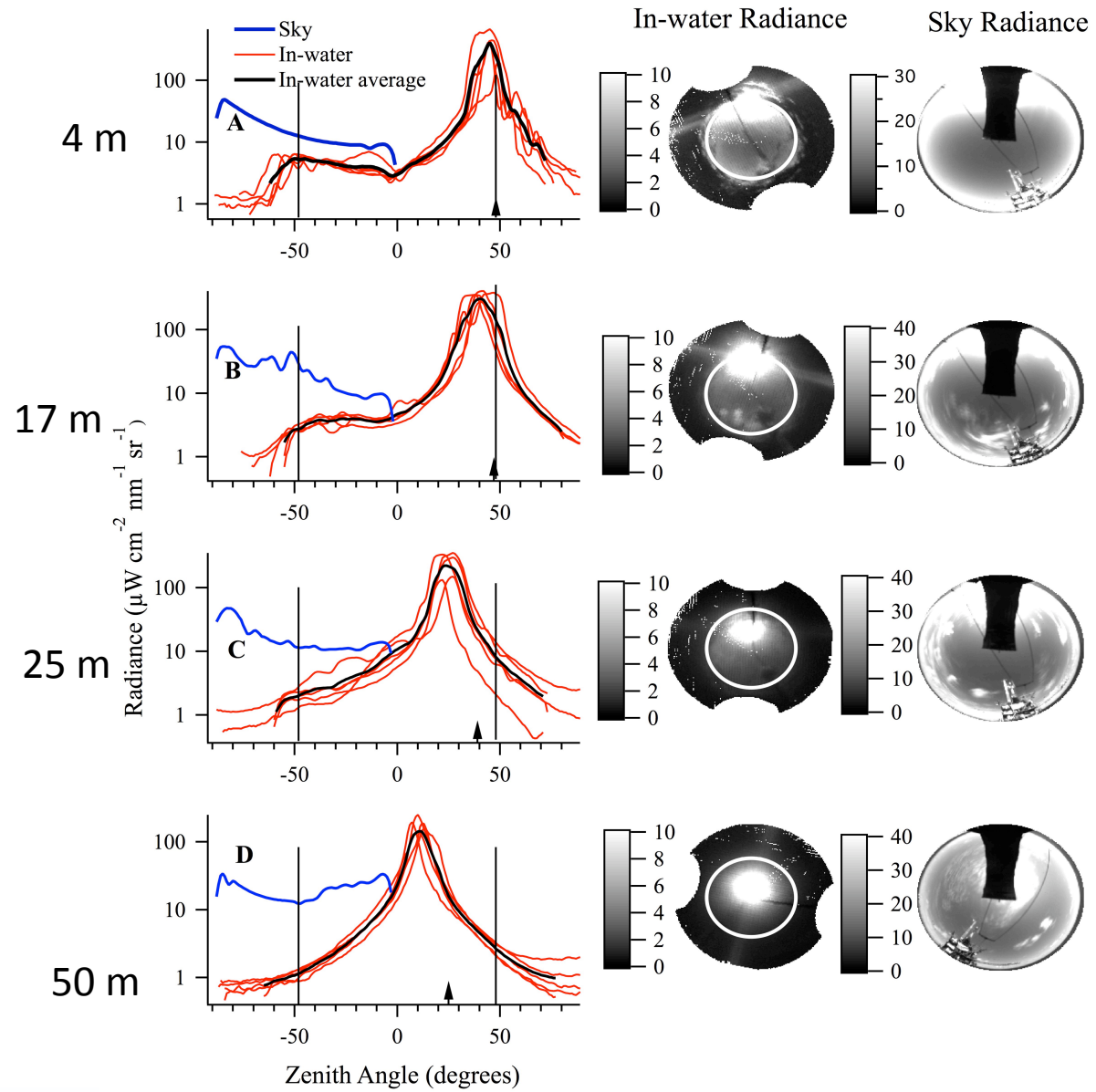


30 m



Radiance Distribution

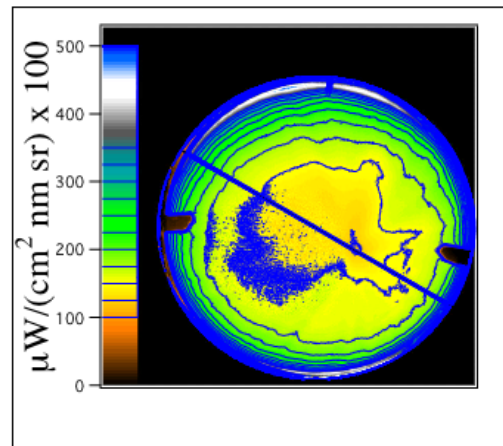
Clear water, Hawaii



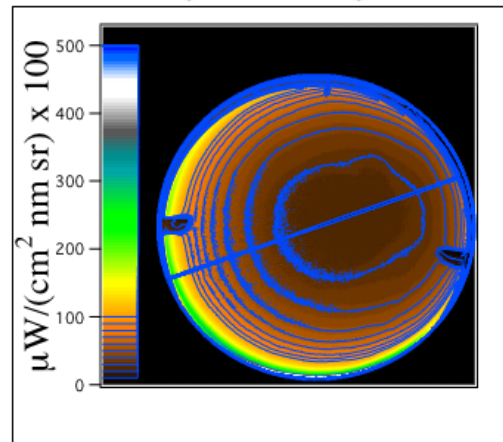
Radiance Distribution

Example Radiance Distribution, 500nm

Low Chl (0.3 mg/m^3)

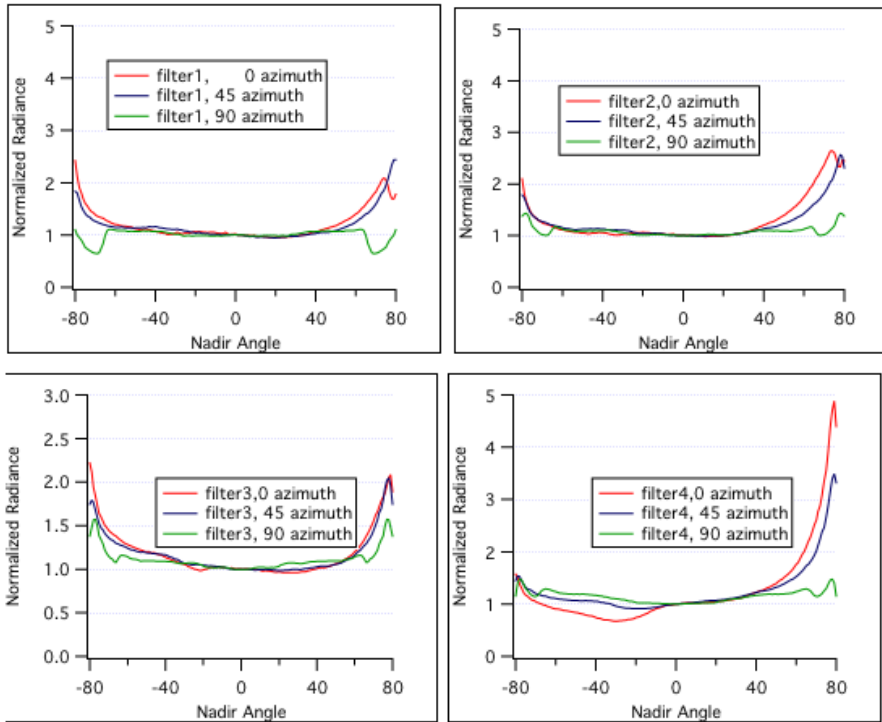


High Chl (5 mg/m^3)

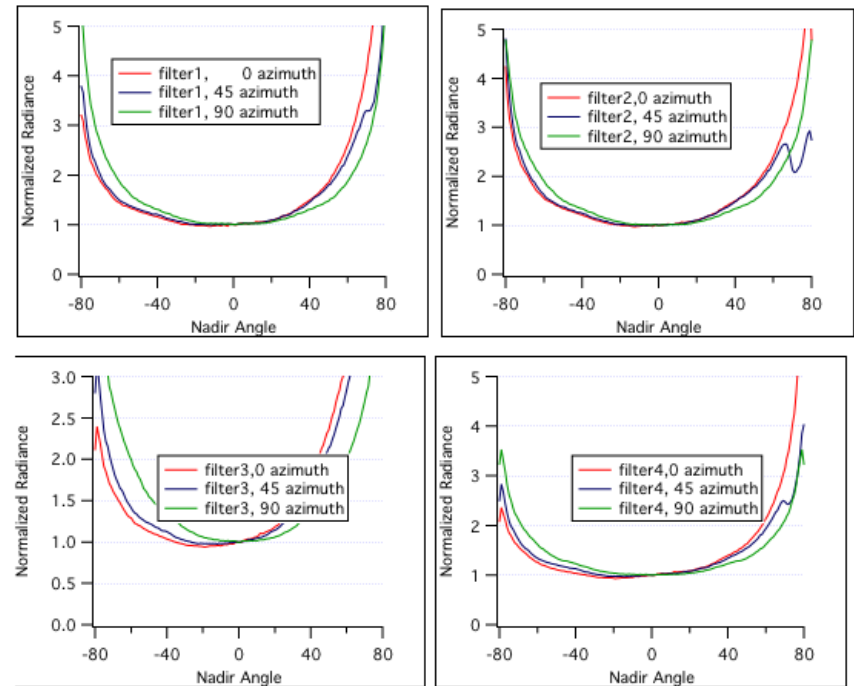


Upwelling Radiance distribution

Low Chl



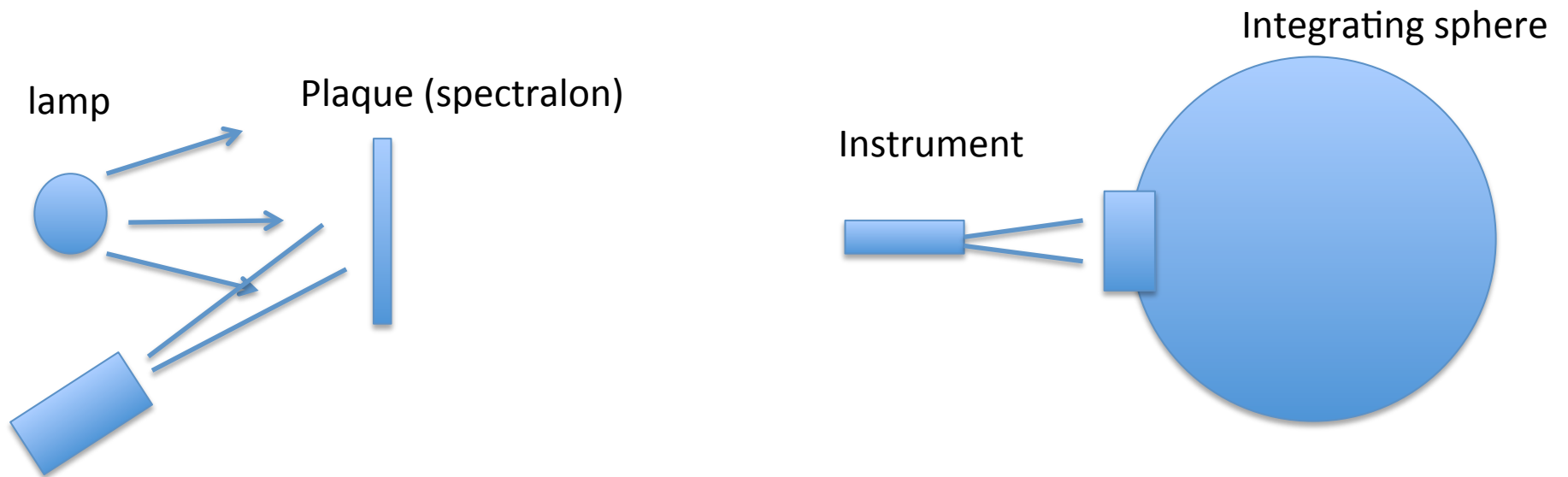
High Chl



Radiance

Calibration: Look at a source of known Radiance

Either bounce light from a lamp off of a plaque, or look into an integrating sphere.



Instrument

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Note how radiance works from plaque, $L = E/\pi$



Calibration problems

Different light levels between field and lab

Different colored sources between field and lab

Different temperatures in lab and field (variation in field temperatures)

Scattered light in lab

Geometrical setup in lab

Drifts in calibration sources

Etc.....

RRS techniques

Want something to relate to satellite measurements, and is an apparent optical property (relatively dependent on water properties, less on illumination conditions):

Remote sensing reflectance

$$R_{rs} = L_w/E_s$$

L_wwater leaving radiance (above surface)

E_sdownwelling irradiance

RRS techniques

Above water techniques:

$$Rrs = Lw / Es$$

$$Rrs = (L_{\text{measured}} - L_g) / Es$$

$$L_g = L_{\text{sky}} * \text{Reflectivity of surface}$$

Reasonable Reflectivity is 0.028 of sky measurement with a geometry of nadir angle 40 deg, azimuth 135 from sun, wind <5 m/s (around 10 knts) (Mobley, 1999) :

References:

Mobley, Estimation of the remote-sensing reflectance from above-surface measurements, Applied Optics, 7442-7455, 1999.

Lee et al., Removal of surface-reflected light for the measurement of remote-sensing reflectance from an above-surface platform, Optics Express, 26313-26324, 2010.

Garaba et al., Comparison of remote sensing reflectance from above-water and in-water measurements west of Greenland, Labrador Sea, Denmark Strait, and west of Iceland, Optics Express, 15938-15950, 2013

In water techniques:

$$R_{rs} = L_u(z) T_{aw} / (E_s * T(z))$$

Measure upwelling radiance at some depth ($L_u(z)$)

Propagate to the surface $T(z) = \exp(-KL(z))$

Propagate through the air-water interface, $T_{aw} (0.975/n^2 = 0.543)$

Measure E_s above the surface

Reference: many...one example Voss et al., An Example Crossover Experiment for Testing New Vicarious Calibration Techniques for Satellite Ocean Color Radiometry, JAOT, 2010.

Also protocols

New Lee technique

Shade surface, measure above the water. Should be directly L_w/E_s

Lee et al. Robust approach to directly measuring water-leaving radiance in the field, Applied Optics, 1693-1701 (2013).

Another factor:

Normalized water leaving radiance

$$nL_w = L_w/E_s * E_o/r^2$$

E_o extra terrestrial solar irradiance

r = earth sun distance

Lee et al. Robust approach to directly measuring water-leaving radiance in the field, Applied Optics, 1693-1701 (2013).