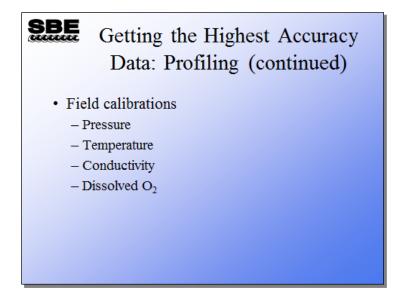
Module 8

Getting the Highest Accuracy Data, Continued

Overview

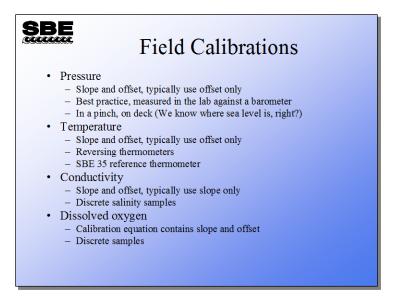


We are going to continue our discussion of methods to ensure the accuracy of profiling equipment, and then we will discuss data from autonomous profilers. We will see that the human influence on conductivity sensors is the greatest obstacle to good conductivity data.

At the end of this module, you should be able to:

- Field calibrate your CTD and Dissolved O₂ sensors.
- Have heightened awareness about the handling of your conductivity sensor.

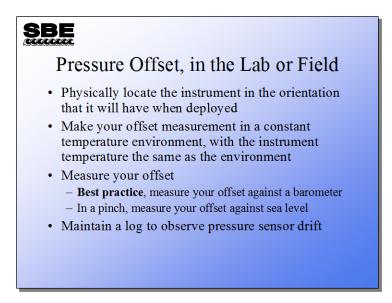
Field Calibrations



The configuration (*.con* or *.xmlcon*) file has entries for *slope* and *offset* for all standard sensor types except dissolved oxygen. These entries are the means to make adjustments in the sensor calibration by using field observations.

The configuration file does not have *slope* and *offset* entries for dissolved oxygen sensors. For the SBE 43, the calibration coefficients *Soc* and *Voffset* are adjusted through comparison to Winkler titrations of discrete samples. For older oxygen sensors, *Soc* and *Boc* are adjusted.

Field Calibrations: Pressure

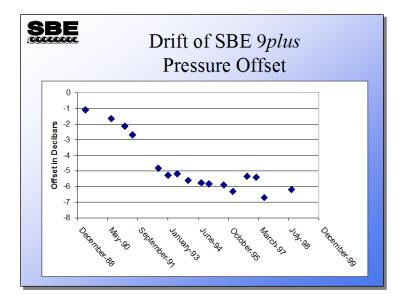


This discussion is primarily intended as a guide for the SBE 9*plus* with a Digiquartz pressure sensor. However, the technique is sound for all pressure sensor types regardless of sensitivity.

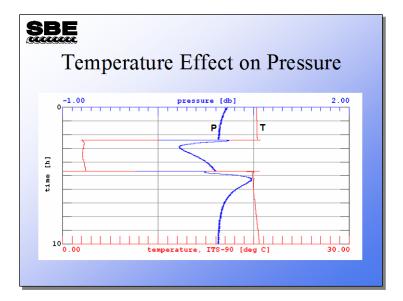
All pressure sensors are sensitive to their orientation, primarily because of gravity's pull on the fluids that fill their capillaries. To correct for this orientation effect, determine the offset with the instrument in the same orientation that it will have when you deploy it.

Pressure sensors exhibit a transient change in their output in response to changes in their environmental temperature. Sea-Bird instruments are constructed to minimize this by thermally decoupling the sensor from the body of the instrument. There is still some residual effect, and the instrument should be allowed to equilibrate in a reasonably constant temperature environment.

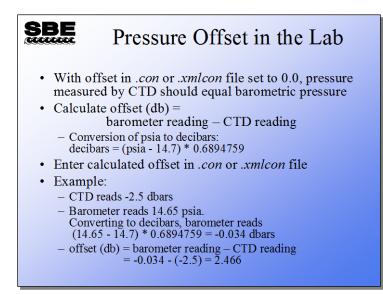
Measure the offset required to zero the pressure sensor with a barometer and convert to decibars for the entry in the *.con* or *.xmlcon* file. As the next slide shows, a log of these offsets can provide good confirmation about the drift rate and show when the sensor needs maintenance.

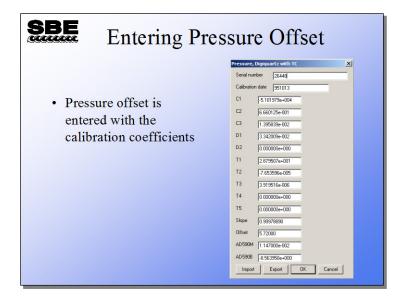


This sensor shows a typical drift until October 1995, when it begins to change in a more random manner. The random behavior indicates that it is time for a calibration and test by the factory.



As we mentioned earlier, the SBE 9*plus* pressure sensor exhibits small pressure excursions in response to rapid changes in temperature. If you are attempting to determine an offset for the pressure sensor in the field, you must take care that the instrument is equilibrated in temperature with its environment. As the plot shows, if you pull the instrument up from a very cold depth, it can take 4 to 5 hours for the pressure sensor to completely equilibrate. It is for this reason that Sea-Bird recommends a laboratory determination of offset in relation to a barometer.





Field Calibrations: Temperature

SBE Field Calibrations, Temperature Mercury deep sea reversing thermometers

read to ± 0.001 °C

- have an accuracy of ± 0.002 °C
 Electronic deep sea reversing thermometers have an accuracy of ± 0.002 °C, but can be
- SBE 3 has an accuracy of ± 0.001 °C
- SBE 35 has an accuracy of > 0.001 °C

Traditional mercury deep-sea reversing thermometers are not capable of resolving temperature accurately enough to field calibrate the SBE 3. Nor do electronic deep-sea reversing thermometers have the accuracy for field calibrations. Sea-Bird markets a deep-sea standards thermometer, the SBE 35, which has the physical configuration to allow calibration in a triple point cell or a gallium melt cell.

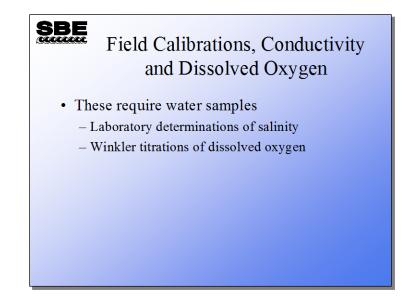
However, you have to be very careful making field calibrations of deep-sea thermometers, because the distance between the two thermometers can make a great difference in the water they measure. Additionally, the part of the ocean used for comparison must change temperature very slowly, to avoid artifacts due to location on the sampling package and time constants.

A further difficulty is that the part of the ocean that changes most slowly is the deepest and coldest part. This means that field calibrations may be carried out over a small part of the temperature range of interest. The paper cited below discusses the authors' experiences and the issues discussed above.

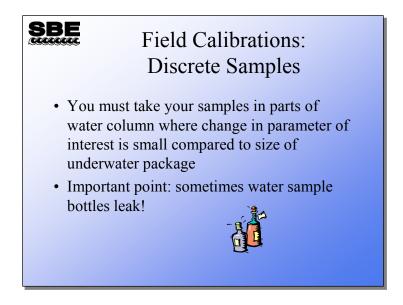
It is best to use pre- and post-cruise calibrations for correction of temperature data.

In-situ Temperature Calibration: A Remark on Instruments and Methods, G. Budeus and W. Schneider, Alfred-Wegener-Institut für Polar- und Meeresforschung, Bremerhaven, Germany, Int. WOCE Newsletter, #30, March 1998, 16-18.

Field Calibrations: Conductivity and Dissolved Oxygen



Field Calibrations: Discrete Sampling



Most instrument packages are more than a meter tall. If you take your samples for field calibrations in a part of the water column where the salinity or oxygen concentration is changing rapidly, you will not get a good sample for calibrating. Not only is there mixing of the water inside the water sampler, but you will be comparing a large mixed sample with a virtual point sample from the sensors.

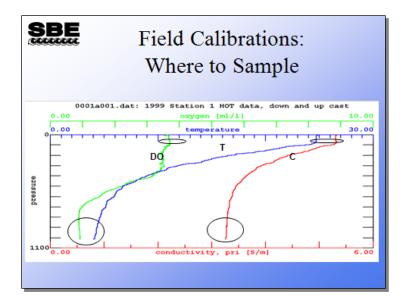
Often the surface of the ocean is well mixed and provides good field calibrations for one end of the scale. And the deep ocean offers plenty of water where salinity and oxygen is changing very slowly for the other end of the scale.

Field Calibrations: Discrete Sampling (continued)

Field Calibrations: Checking for Leaks
Run underwater package down deep to nice, uniform water
Close all water bottles
Run salinities on each water bottle
Compare salinities, fix leakers, and repeat

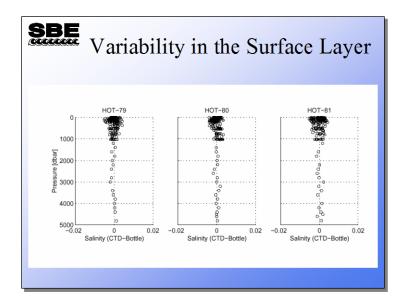
A water bottle consists of a plastic tube with top and bottom caps. The caps are sealed with o-rings and held in place with a spring or elastic tube. Consider that the instrument package moves through the water column on average at 1 meter per second, and faster when the ship heaves. Leaky o-rings or weak springs can allow an exchange of water between the captured sample and the ocean as the instrument package is brought to the surface. It is good practice to take the instrument package down to a depth where the salinity is changing very slowly, and then close all the sample bottles. Using this method, any leakers will be obvious when the laboratory salinity samples are run. Repair or replace any bottles that leak, or only use bottles that have been shown not to leak in field calibrations.

Field Calibrations: Discrete Sampling (continued)



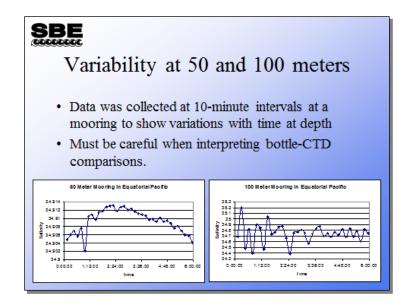
Use samples from depths showing the most uniformity in the parameter you are most interested in.

Field Calibrations: Conductivity



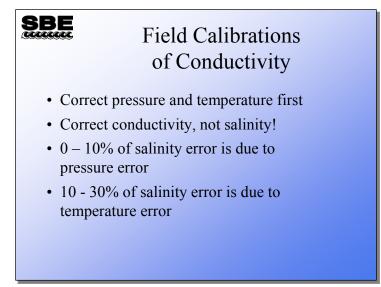
These data are taken from 3 cruises off Hawaii. The problem with using the surface layer to correct CTD conductivity is obvious.

L. Tupas, et al., Hawaii Ocean Time-series Data Report 9, 1997. University of Hawaii, School of Ocean and Earth Science and Technology. page 21

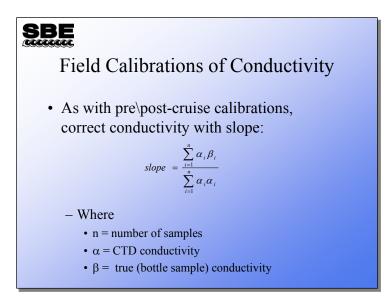


This slide shows data from a mooring near the equator. The 50-meter mooring data shows a change in salinity that might be from tidal influence. The change observed here is of similar magnitude to the correction that might be applied to CTD data based on the difference between discrete samples and the CTD.

The 100-meter mooring data shows changes in salinity that might be caused by internal waves in the thermocline. Changes of this magnitude over this time interval will cause a large and real difference between the upcast and downcast.



Because the equation that converts the conductivity sensor output from frequency to conductivity includes pressure and temperature as well as frequency, it is necessary to correct pressure and temperature before correcting conductivity. The usual reason for collecting conductivity data is to calculate salinity. Examining the salinity equation, up to 10% of a possible salinity error could be in the pressure term, 10 - 30% in the temperature term, and the remainder in the conductivity term. It is well worth correcting pressure and temperature in addition to conductivity.



The summation symbol, Sigma (Σ), denotes the addition of a series of values. The script on the bottom of the Σ is the index of the starting value, the script on the top is the ending value. We wish to use all suitable samples so we will start with one and end with n, the total number of samples.

Example:

Suppose we had 2 salinity samples to go with our CTD cast. The salinity of these water samples is determined by a laboratory salinometer. Using SeaCalc II, the salinity is paired with the corresponding corrected temperature and pressure data from the CTD cast, and the conductivity of the salinometer samples is calculated.

CTD Conductivity (α)	Salinometer Conductivity (β)
2.1234	2.1244
4.1234	4.1244

 $slope = \frac{(2.1234 * 2.1244) + (4.1234 * 4.1244)}{(2.1234 * 2.1234) + (4.1234 * 4.1234)}$

slope = 1.00029

S	• Raw data is shown below								
		at CTD te	emperatur	e shown					
	is ITS-9	90							
	CTD	CTD	CTD	CTD	Bottle				
	pressure	temperature	conductivity	salinity	salinity				
	202.7	18.3880	4.63421	34.9705	34.9770				
	1008.8	3.9831	3.25349	34.4634	34.4710				
	4064.1	1.4524	3.16777	34.6778	34.6850				

This example is a slight variation of the example in **Application Note 31**. You would find the CTD data in your *.ros* file, which is created by the Data Conversion module.

SBE Step One: Conductivity Correction										
	 Correct P for +0.5 dbar error Correct T for +0.0015 °C error Recalculate CTD salinity for comparison to Bottle salinity 									
(Corrected Corrected CTD CTD Bottle CTD CTD conductivity salinity salinity pressure tamperature CTD CTD corrected salinity									
	CTD pressure	CTD temperature	conductivity	salinity (T, P corrected)						
			conductivity 4.63421	-						
	pressure	temperature		(T, P corrected)	salinity					

Temperature and pressure are corrected first. CTD salinity is recalculated only for comparison to the bottle salinity. We will be correcting conductivity, not salinity.

SE									
	Step Two: Conductivity Correction								
	 Bottle conductivity is calculated at CTD corrected T and P using SeaCalc III Note slope shown in CTD – Bottle conductivity 								
	Note slope slov		le conductivity						
	CTD	Bottle	CTD – Bottle						
	-								
	CTD	Bottle	CTD - Bottle						
	CTD conductivity	Bottle conductivity	CTD – Bottle conductivity						
	CTD conductivity 4.63421	Bottle conductivity 4.63481	CTD – Bottle conductivity -0.00060						

The numbers in the column labeled $CTD - Bottle \ conductivity$ are not constant. Rather, they have the slope we have been harping on.

Let's look at calculating the slope:

$$slope = \frac{\sum_{i=1}^{n} \alpha_i \beta_i}{\sum_{i=1}^{n} \alpha_i \alpha_i}$$

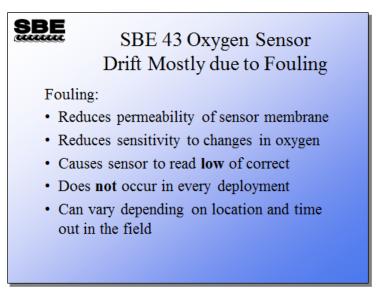
Slope =

 $\frac{(4.63421 * 4.63481) + (3.25349 * 3.25398) + (3.16777 * 3.16822)}{(4.63421 * 4.63421) + (3.25349 * 3.25349) + (3.16777 * 3.16777)} = 1.000138$

S	SBE Step Three: Conductivity Correction								
•	Slope calculated from previous slide is 1.000138								
•	 Place slope in slope entry of conductivity calibration coefficients; Corrected CTD conductivity = CTD conductivity * slope 								
•		hity is calculated from here, and corrected ter	corrected CTD nperature and pressure						
	Corrected CTD conductivity	Corrected CTD salinity	Bottle Salinity						
	4.63485	34.9773	34.9770						
	3.25394	34.4706	34.4710						
	3.16821	34.6849	34.6850						

The correction puts the CTD salinities much closer to the bottle salinities. You may be wondering what to do if you collect bottle salinities with every cast and have many casts in a cruise. It would be a bit onerous to make this calculation for every cast and process each cast with a different slope. Usually, making this calculation and changing the slope value in the conductivity sensor's calibration coefficients each week is sufficient. However as we have discussed, fouling is often *an event*. This being the case, careful scrutiny of your data is warranted to ensure that you catch these events and change the slope correction accordingly.

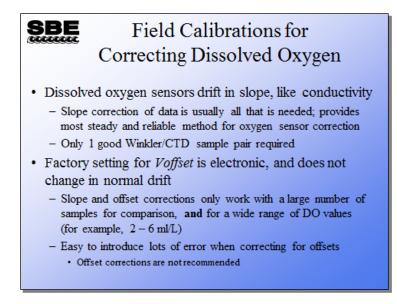
Field Calibrations: Dissolved Oxygen



There are two mechanisms at work when it comes to SBE 43 oxygen sensor drift:

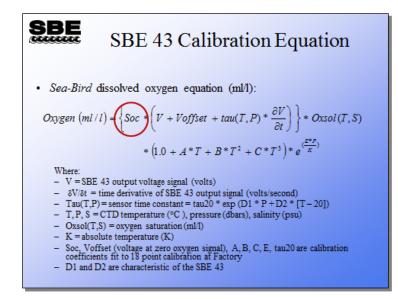
- The primary cause of sensor calibration drift is **fouling** of the sensor membrane. This can be a slow change over time, as the membrane accumulates oils and other materials during cruises and long deployments. Fouling can also occur in an event, such as after passing through an oil slick or impaling a jelly fish. Following recommended cleaning procedures can take care of most fouling problems (see Application Note 64).
- 2. A lesser concern is electrolyte consumption. The SBE 43 is continuously polarized, so will continue to react with oxygen in its plenum housing when not sampling in the water, unless the oxygen supply is choked off. Though this process is reduced by the semi-enclosed housing of the DO sensor, we do recommend that after cleaning the sensor, that it be stored with a closed loop of Tygon tubing. Enclose with a small piece of damp sponge inside the tubing if there is no risk of freezing. We do not recommend storing the SBE 43 in water, as this can lead to *in situ* fouling.

Field Calibrations: Dissolved Oxygen



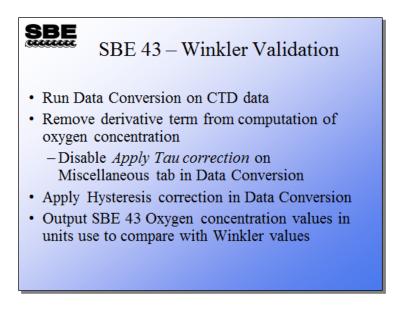
Terms that can be modified by the user to adjust the calibration of the SBE 43:

- *Soc* only (*Soc* can change in time due mostly to fouling)
- Soc and Voffset together (Soc can change in time due mostly to fouling)
- *E* calibration constant
 - The factory value is determined at 0 db and works well for most, but can be adjusted by the user.
 - This is a one-time correction determined using deep pressure sensor and water sample comparison taken at depths > 1000 m.



What one needs to consider in the Sea-Bird DO calibration equation:

- The basis for calculating dissolved oxygen is a modified version of the algorithm from Owens and Millard (1985), referred to in our software as the *Sea-Bird* algorithm or *Sea-Bird Calibration Equation*.
- The calibration slope term *(Soc)*, which changes as the sensor sensitivity is modified, typically by fouling, is the coefficient we are most concerned with.
- An electronic offset term (*Voffset*) related to the voltage output observed at a zero oxygen signal is unique to each sensor and is constant.
- A third-order polynomial component that compensates for changes in the sensor's sensitivity as a function of temperature remains constant.
- An exponential term that compensates for the instantaneous changes in the sensitivity of the sensor with changes in pressure (*E*) can be modified to fine tune deep-ocean oxygen data (covered in more detail later in this module).



The tau (T,P) * δV/δt term is proportional to the first derivative of the oxygen sensor output voltage. This term is introduced to sharpen the response of the sensor to rapid changes in oxygen concentration. However, it also amplifies residual noise in the signal (especially in deep water), and in some situations this negative consequence overshadows gains in signal responsiveness. To remove the derivative term, disable *Apply Tau correction* on the Miscellaneous tab in Data Conversion; deleting tau (T,P) * δV/δt from the equation.

	Hysteresis and Tau ed in Data Conversion
concentrations uppin	A Conta Conversion
	File Setup Data Setup Miccellaneous Header Vervi
	This tab configures miscellaneous data for calculations. Note: Values entered only affect indicated calculations.
	Depth and Average Sound Velocity
Oxygen, SBE 43	Latitude when NMEA is not available
Serial number 0603	Average Sound Velocity Plume Aromaly
Calibration date 23-sep-2007	Minimum pressure (db) (20 Theta-B (0
les apressi	Minimum salinity (pru) [20 Salinity-8 [0
C Use Owens-Millard Equation	Pressure window size (db) 20 Theta-Z / Salinity-Z 0
Use Sea-Bird equation only for SBE calibration in 2008 and later	Time window size [s] [60 Reference pressure [db] [0
calibration in 2008 and later	Descent and Acceleration
Soc 0.3874 D1 1.92534e-004	Window size [1] [2
Volfset 525000e.001 02 454803e.002	Queen
	Window size [1]
A -2.95900e-004 H1 -3.30000e-002	P Apply Tau connection
B 1.40130e-004 H2 5.00000e+003	Apply hysteresis correction to SBE 43 when Sea-Bild equation selected in .con file
C 336160e-006 H3 145000e+003	Potential Temperature Anomaly
	A0 0 A1 0 A1 Multipler Salinity .
E 3.60000e-002	an and
Tau20 1	Set to Defaults
Import Export OK Carcel	Start Process Ext Carcel
Import Export OK Cancel	

A time-dependent hysteresis effect on the sensor membrane affects the membrane permeability by plasticization of the polymer membrane and modification of the ratio of crystalline and amorphous components in the membrane. This affects at all depths, but becomes significant when deeper than 1000 meters. This is not dealt with in the calibration equation term E. Instead, deep-ocean hysteresis is corrected for separately as it requires a series of time-dependent functions not accommodated in the Sea-Bird calibration algorithm.

To perform deep-water hysteresis corrections on your SBE 43 oxygen data, select *Apply hysteresis correction to SBE 43 when Sea-Bird equation selected in .con or .xmlcon file* on the Miscellaneous tab in the Data Conversion dialog box. Ranges and default values for the hysteresis correction are:

- H1 amplitude, range -0.03 to -0.05, **default = -0.033**.
- H2 non-linear component, does not require tuning between sensors, **default = 5000**.
- H3 time constant, range 1200 to 2000 sec, default = 1450 sec.

These parameters can be adjusted if needed for high accuracy applications, but default values typically produce excellent results.

Hysteresis responses of membranes on individual SBE 43 sensors are very similar; in most cases the default parameters provide the accuracy specification of within 2% of true value. For users requiring higher accuracy ($\pm 1 \mu mol/kg$), the parameters can be fine-tuned if a complete profile (descent and ascent) made preferably to > 3000 meters is available. Hysteresis can be eliminated by alternately adjusting H1 and H3 in the .con or .xmlcon file during comparison of the complete profile with corresponding Winkler water sample values. Once established, these parameters should be stable, and can be used without adjustment on other casts collected using the same SBE 43.

Perform hysteresis corrections to deep profile data being used to modify the *Soc* term.

SBE

SBE 43 – Winkler Validation

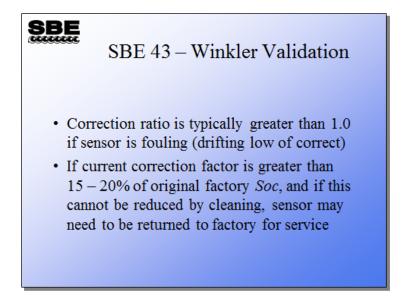
- Choose depth of CTD and Winkler water sample comparisons where D.O. is not changing much

 Collect replicate field samples if possible, and use
 - average or "best of"
- If replication not possible, collect samples at multiple locations to get idea of sampling variability and to be sure you do not have a bad sample
- Near surface and low oxygen Winkler samples will have higher standard deviations

Correcting SBE 43 DO Data using Field Validation Requires Care:

- Field validations must be carefully executed!
- Things that can contribute to sensor differences from water sample values besides sensor calibration drift or malfunction:
 - Mismatched depths between sensor and bottles
 - Internal waves
 - Non-equilibrated sensor/bottle (not long enough wait time prior to closing bottles)
 - Steep gradients over length of sampling package
 - Poor QA on Winkler titrations (chemicals, blanks, sample draw errors, bubbles in samples, analyst)

SBE 43 – Winkler Validation Compare a Winkler value and corresponding SBE 43 value (corrected for deep-ocean hysteresis in Data Conversion) Compute correction ratio = (Winkler value / SBE 43 Value) Multiply factory *Soc* by ratio to get *newSoc*Replace factory *Soc* in .con or .xmlcon file with *newSoc*Process data from time of correction forward with *newSoc OR multiply SBE 43 output values by correction ratio to get slope corrected data.*

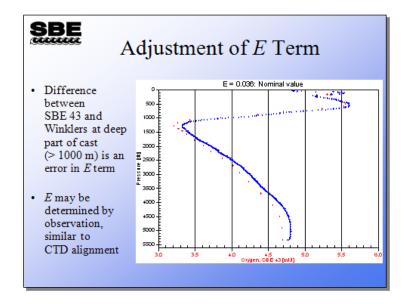


When is a change in *Soc* indicating the sensor needs to be serviced, cleaned, or recalibrated at the factory?

- The correction ratio is typically greater than 1.0 if the sensor is fouling as the loss of sensitivity requires increasing *Soc* to give the correct DO values.
- If the correction factor is greater than 15-20% of the original factory *Soc* (ratio of Winkler/SBE 43 ~ 1.2), and when this cannot be reduced by cleaning, the sensor may need to be returned to the factory for service.
- Other options for data correction are discussed in several papers on our website.
- An exercise in Module 12 is provided to demonstrate this method of DO data correction in a moored application.
- For additional information on SBE 43 data and corrections, see **Application Notes 64, 64-1, and 64-2** on our website.

Field Calibrations: Dissolved Oxygen Pressure Effects

Adjusting *E* in the Calibration Equation (*continued*)



The term in the equation that corrects for pressure effects has little effect in the upper part of the profile. The slide above illustrates that as the pressure increases, the response of the instrument deviates from the Winkler titrations. We can improve the agreement of the SBE 43 and the Winkler titrations by adjusting E. The instantaneous effect of pressure on the sensor membrane permeability is captured in the E term of the calibration equation.

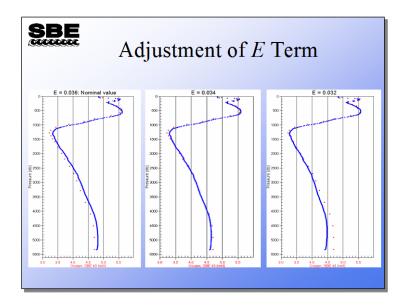
- Necessary for all profile data, regardless of deep or shallow water.
- *E* can be adjusted so data are fit to Winkler samples after conducting hysteresis corrections.

Field Calibrations: Dissolved Oxygen Pressure Effects Adjusting *E* in the Calibration Equation (*continued*)

figuration for	the SBE 911plus/917plus CTD						
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eck unit or SEARA	M SBE11plus Firmware Versi	ion >= 5.0 •	Calibratio	n date	27-Mar-200	7	_
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NMEA device co		s added				D1	32 <u></u>
NNEA device co				4.7900			1.92640e-004
Surface PAR vol	resolved to PC	added	Soc	4.7900	0e-001		1.92640e-004
Surface PAR vol	Inge added ID PC		Soc		0e-001	D1	32 <u></u>
Surface PAR vol Channel Frequency	Intercented to PC	added	Soc Volfset	4.7900	0e-001 00e-001	D1 D2	1.92640e-004
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Surface PAR vol Channel Frequency Frequency Frequency Frequency A/D voltage 0	Ange added Sensor Sensor Temperature Conductivy Pensore, Digiquatz with TC Firee	added Open Sove	Soc Volfset A	4.7900 -5.2560 -3.9090 1.9000	0e-001 00e-001 00e-004	D1 D2 H1	1.92640e-004 -4.17760e-002 -3.30000e-002
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Surface PAR vol Channel Frequency Frequency Frequency Frequency AvD voltage 0 AvD voltage 1 AvD voltage 2	Avected b PC Tage added C Sensor Temperature Conductivity Persues, Digguate with TC Free Free Free Free Free Free Free Fre	edded New Open Seve Az Select	Soc Volfset A B	4.7900 -5.2560 -3.9090 1.9000	0e-001 00e-001 00e-004 0e-004 00e-006	D1 D2 H1 H2	1.92640e-004 -4.17760e-002 -3.30000e-002 5.00000e+003
Surface PMR vol Channel Frequency Frequency Frequency Frequency A/D voltage 0 A/D voltage 1 A/D voltage 3	Interded 55 PC Isge added IF Scan time Sensor Encodectivity Pressue, Diggastz with TC Free Free Free Free Free Free Free Fre	edded New Open Seve Az Select	Soc Volfset A B C	4.7900 -5.2560 -3.9090 1.9000 -2.0000	0e-001 00e-001 00e-004 0e-004 00e-006	D1 D2 H1 H2	1.92640e-004 -4.17760e-002 -3.30000e-002 5.00000e+003
Surface PAR vol Channel Frequency Frequency Frequency Frequency	Avented to PC tage added F Scout time a Sonice Sonice Conductivity Pensure, Togiquatz with TC Free Free Free Free Free Free Free Fre	edded New Open Seve Az Select	Soc Volfset A B C E	4.7900 -5.2560 -3.9090 1.9000 -2.0000 3.6000	0e-001 00e-001 00e-004 0e-004 00e-006	D1 D2 H1 H2	1.92640e-004 -4.17760e-002 -3.30000e-002 5.00000e+003

Field Calibrations: Dissolved Oxygen Pressure Effects

Adjusting *E* in the Calibration Equation (*continued*)



We can make the adjustment to *E* empirically. The plots above show the discrepancy between the SBE 43 calculated oxygen and the Winkler titrations with a series of *E* values. Clearly, the middle value of E = 0.034 gives the best agreement.

Activity: Correct CTD Conductivity with Water Samples

Pressure db	CTD Temp (ITS-90)	Cond	Uncorrected CTD Salinity	Water Bottle Salinity	Water Bottle Cond	Corrected CTD Temp (ITS-90)	Corrected CTD Cond	Corrected CTD Salinity	Corrected CTD Salinity- Water Bottle Salinity
4.9	24.0798	5.23638	35.1885	35.2055		24.0798			
519	6.6922	3.43991	34.0769	34.0848		6.6922			
850.6	4.4142	3.27659	34.3667	34.3738		4.4142			
1000.8	4.003	3.25475	34.4616	34.472		4.003			
1202.3	3.5221	3.22482	34.5083	34.5148		3.5221			
1401	3.039	3.19378	34.5452	34.5503		3.039			
1599.6	2.6724	3.1719	34.5692	34.5769		2.6724			
1999.1	2.1309	3.1445	34.6131	34.6194		2.1309			
2400.2	1.7884	3.13273	34.6392	34.6463		1.7884			
2798.9	1.5911	3.13234	34.6563	34.6645		1.5911			
3200.1	1.4927	3.1397	34.6674	34.676		1.4927			
3600.3	1.4587	3.15175	34.6737	34.6829		1.4587			
4001.5	1.4537	3.16568	34.6772	34.6853		1.4537			
4401.9	1.4766	3.18142	34.6790	34.6871		1.4766			
4500.7	1.4868	3.18558	34.6788	34.6883		1.4868			
4600.8	1.4969	3.18976	34.6789	34.6883		1.4969			
4809.4	1.5119	3.19792	34.6795	34.6884		1.5119			

1. What temperature scale is CTD temperature reported in? What temperature scale is used to calculate conductivity?

2. Use SeaCalc III to calculate "Water Bottle Conductivity" using "Corrected CTD Temp" and "Water Bottle Salinity".

3. Calculate a conductivity correction slope based on the shaded portion of the table. We are using 3 data rows in class as a quick exercise. Normally, how much of the table would you use? Recall pages 17 and 20.

CTD Conductivity Corrected With Water Samples

Pressure db	CTD Temp (ITS-90)	Cond	Uncorrected CTD Salinity	Water Bottle Salinity	Water Bottle Cond	Corrected CTD Temp (ITS-90)	Corrected CTD Cond	Corrected CTD Salinity	Corrected CTD Salinity- Water Bottle Salinity
4.9	24.0798	5.23638	35.1885	35.2055	5.23862	24.0798	5.23763	35.1980	-0.0075
519	6.6922	3.43991	34.0769	34.0848	3.44062	6.6922	3.44073	34.0861	0.0013
850.6	4.4142	3.27659	34.3667	34.3738	3.27720	4.4142	3.27737	34.3758	0.0020
1000.8	4.003	3.25475	34.4616	34.472	3.25563	4.003	3.25553	34.4708	-0.0012
1202.3	3.5221	3.22482	34.5083	34.5148	3.22537	3.5221	3.22559	34.5175	0.0027
1401	3.039	3.19378	34.5452	34.5503	3.19420	3.039	3.19454	34.5544	0.0041
1599.6	2.6724	3.1719	34.5692	34.5769	3.17253	2.6724	3.17266	34.5785	0.0016
1999.1	2.1309	3.1445	34.6131	34.6194	3.14502	2.1309	3.14525	34.6223	0.0029
2400.2	1.7884	3.13273	34.6392	34.6463	3.13331	1.7884	3.13348	34.6484	0.0021
2798.9	1.5911	3.13234	34.6563	34.6645	3.13301	1.5911	3.13309	34.6655	0.0010
3200.1	1.4927	3.1397	34.6674	34.676	3.14039	1.4927	3.14045	34.6767	0.0007
3600.3	1.4587	3.15175	34.6737	34.6829	3.15250	1.4587	3.15250	34.6829	0.0000
4001.5	1.4537	3.16568	34.6772	34.6853	3.16634	1.4537	3.16644	34.6864	0.0011
4401.9	1.4766	3.18142	34.6790	34.6871	3.18208	1.4766	3.18218	34.6883	0.0012
4500.7	1.4868	3.18558	34.6788	34.6883	3.18636	1.4868	3.18634	34.6881	-0.0002
4600.8	1.4969	3.18976	34.6789	34.6883	3.19054	1.4969	3.19052	34.6881	-0.0002
4809.4	1.5119	3.19792	34.6795	34.6884	3.19865	1.5119	3.19868	34.6888	0.0004

Note: For Shaded section of table:

Sum of CTD conductivity * Water Sample conductivity = 30.55649 Sum of CTD conductivity * CTD conductivity = 30.54918 Ratio used to correct CTD conductivity = 1.000239